



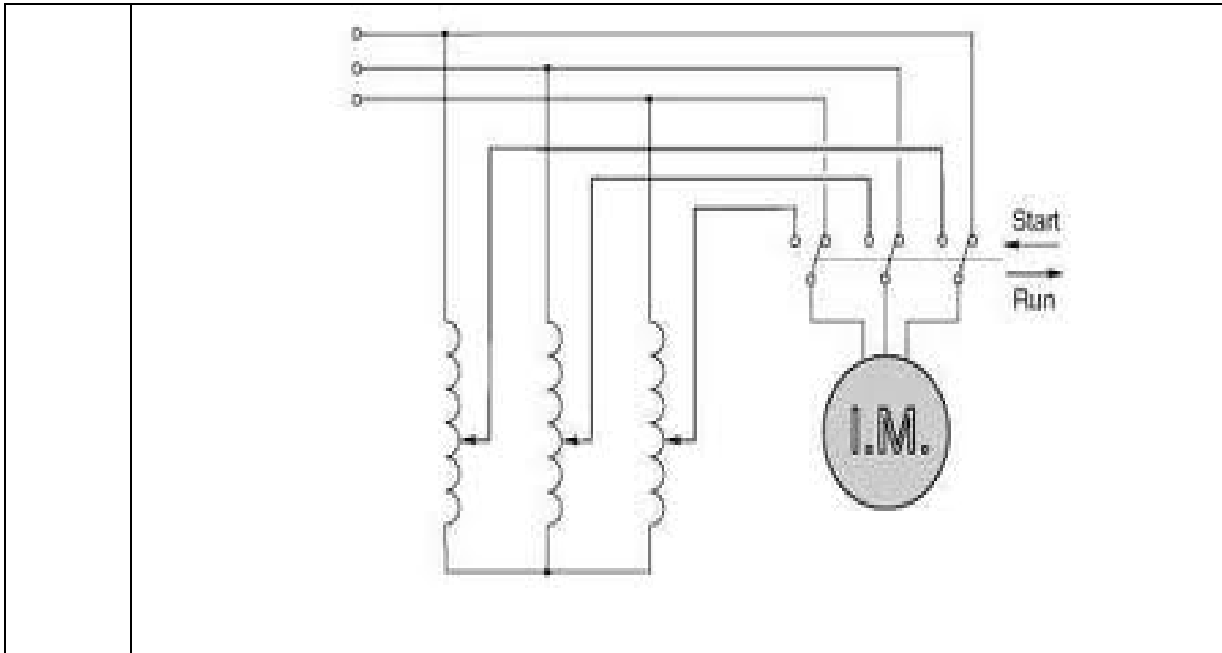
**Important suggestions to examiners:**

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more importance. (Not applicable for subject English and communication skills)
- 4) While assessing figures, examiner may give credit for principle components indicated in a figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
- 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and model answer.
- 6) In case some questions credit may be given by judgment on part of examiner of relevant answer based on candidate understands.
- 7) For programming language papers, credit may be given to any other program based on equivalent concept.

<b>Q.1 A)</b>	<b>Attempt any three of the following:</b>	<b>12 Marks</b>
<b>i)</b>	<b>State why three phase induction motor never run on synchronous speed?</b>	
Ans:	<p style="text-align: right;"><b>(4 Marks)</b></p> <p>The working principle of three phase induction motor is based on relative motion between rotating magnetic field and rotor conductors i.e (<math>N_s - N</math>), According to Lenz's law rotor will try to catch the synchronous speed of rotating magnetic field to oppose the 'cause producing it'. But rotor never succeeds due to frictional losses.</p> <p>If rotor catches the synchronous speed of rotating magnetic field, (<math>N_s - N</math>) i.e relative motion will be zero and rotor stops to rotate and therefore three phase induction motor can never run on synchronous speed .</p> <p style="text-align: center;"><b>OR</b></p> <p>Relative motion between rotor conductors and rotating magnetic field induces rotor currents. Interaction of rotor current of stator flux produces torque on rotor which means that relative motion of rotor is the cause of rotation of rotor. In No-load condition, due to friction of Windage rotor has to produce a small torque to overcome frictional force and thus rotor speed never catches synchronous speed .</p>	



<p>ii)</p> <p>Ans:</p>	<p><b>State the effect of rotor resistance on torque of an induction motor.</b></p> <p><b>Characteristics:</b> <span style="color: red;">(2 Mark Characteristics &amp; 2 Mark Effect)</span></p> <div data-bbox="581 443 1227 863"><p style="text-align: center;"><b>Equivalent Characteristics</b></p></div> <p><b>Effect:</b></p> <ul style="list-style-type: none"><li>➤ When rotor resistance increases, maximum torque condition occurs at higher values of slip and characteristics shifts towards left hand side.</li><li>➤ The maximum torque condition can be obtained at any required slip by changing rotor resistance.</li></ul>
<p>iii)</p> <p>Ans:</p>	<p><b>Draw a neat diagram for Autotransformer starter used in 3 phase induction motor.</b></p> <p><b>Diagram for Autotransformer starter :</b> <span style="color: red;">( 4 Marks)</span></p> <div data-bbox="537 1283 1256 1808"></div> <p style="text-align: right;">OR</p>



iv) **State the necessity of AC generator. State any two parts of AC generator with material used for them.**

Ans: **Necessity of AC generator: (2 Mark)**

- In India the transmission and distribution system of electrical energy is based on three phase &, single phase AC voltages therefore the generation of three phase AC voltages is to be done.
- For this purpose AC generator is required. In India, in the most of the power generating stations, AC generator is used for generating 3-Ph voltages.

**Basic parts of AC generator: (1 Mark)**

1. Armature System:
2. Field System

**Material Used in AC generator: (1 Mark)**

1. Armature: Copper/Aluminum wire for armature winding and silicon steel laminations for armature core
2. Field : Silicon steel laminations for field pole core, copper /Aluminum wire for field winding

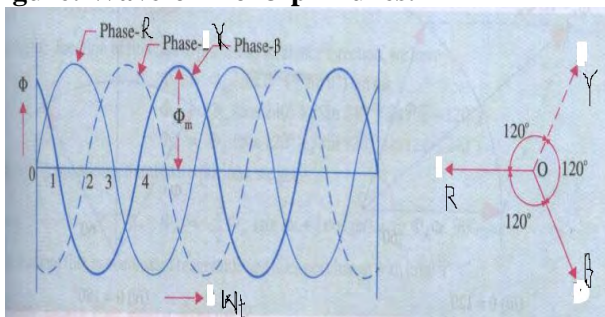
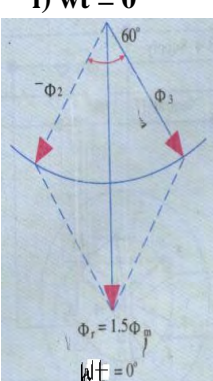
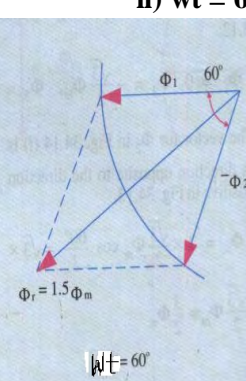
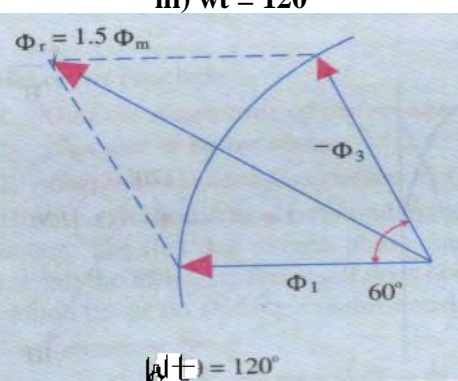


<b>Q.1B)</b>	<b>Attempt any one of the following :</b>	<b>06 Marks</b>
i)	<b>Explain voltage frequency method of speed control of 3 phase induction motor.</b>	
Ans:	<p><b>Figure:</b> <span style="float: right; color: red;">(3 Mark Figure &amp; 3 Mark Effect)</span></p> <p style="text-align: center;"><b>OR Equivalent fig</b></p> <p><b>Explanation:</b></p> <ul style="list-style-type: none"> <li>➤ A simple circuit arrangement for obtaining variable voltage and frequency is as shown in the above figure.</li> <li>➤ This type of control is usually known as Volts/ Hertz or V/f control.</li> <li>➤ If the ratio of voltage to frequency is kept constant, the flux remains constant.</li> <li>➤ The maximum torque which is independent of frequency can be maintained approximately constant.</li> <li>➤ However at a low frequency, the air gap flux is reduced due to drop in the stator impedance and the voltage has to be increased to maintain the torque level.</li> </ul>	
ii)	<b>Draw a schematic diagram of an a.c. series motor. How to change its speed and direction of rotation? Give two applications of a.c. series motors.</b>	
Ans:	<p><b>Schematic diagram of an A.C Series motor:</b> <span style="float: right; color: red;">(2 Mark)</span></p> <p style="text-align: center;"><b>OR</b></p>	



	<p><b>Reason for change its speed:</b> <span style="float: right;"><b>(1 Mark)</b></span></p> <ul style="list-style-type: none"> <li>➤ Since the speed of this motor is not imitated by the supply frequency hence the speed control of this motor is best obtained by solid state devices.</li> </ul> <p><b>Reason for change its direction of rotation:</b> <span style="float: right;"><b>(1 Mark)</b></span></p> <ul style="list-style-type: none"> <li>➤ The direction of rotation can be changed by interchanging connection to the field with respect to the armature.</li> </ul> <p><b>Applications of A.C Series Motor (Any two from following or any similar ) (2 Mark)</b></p> <ol style="list-style-type: none"> <li>1. Where high starting torque is required e.g. Electric Traction</li> <li>2. Stone Crushing Machine</li> <li>3. Washing Machines.</li> <li>4. Mixers and grinders</li> <li>5. Food processors.</li> <li>6. Small drilling Machines.</li> <li>7. In main line service</li> <li>8. In Electric Traction</li> </ol>
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<b>Q.2</b>	<b>Attempt any four of the following :</b>	<b>16 Marks</b>
a)	<b>Explain with neat sketches, the production of rotating magnetic field in three phase induction motor</b>	

<b>Ans:</b>	<p><b>Figure: Waveform of 3-ph fluxes:</b></p>  <p style="text-align: right;"><b>or Equivalent fig.----- (1 Mark)</b></p> <p><b>Vector diagram at</b></p> <div style="display: flex; justify-content: space-around;"> <div style="text-align: center;"> <p><b>i) <math>\omega t = 0</math></b></p>  </div> <div style="text-align: center;"> <p><b>ii) <math>\omega t = 60^\circ</math></b></p>  </div> <div style="text-align: center;"> <p><b>iii) <math>\omega t = 120^\circ</math></b></p>  </div> </div> <p style="text-align: right;"><b>or Equivalent fig. ----- (2 Marks)</b></p>
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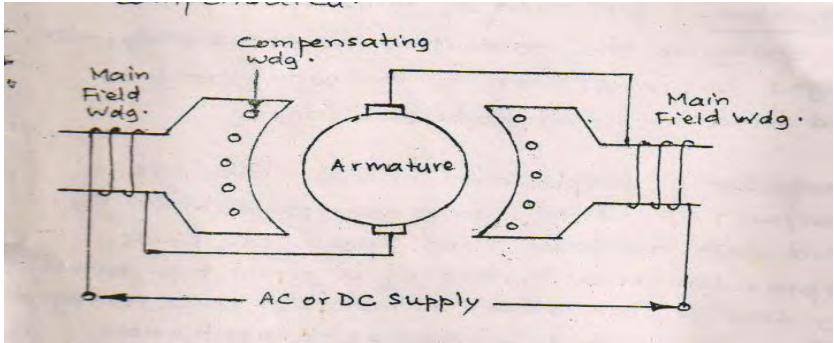
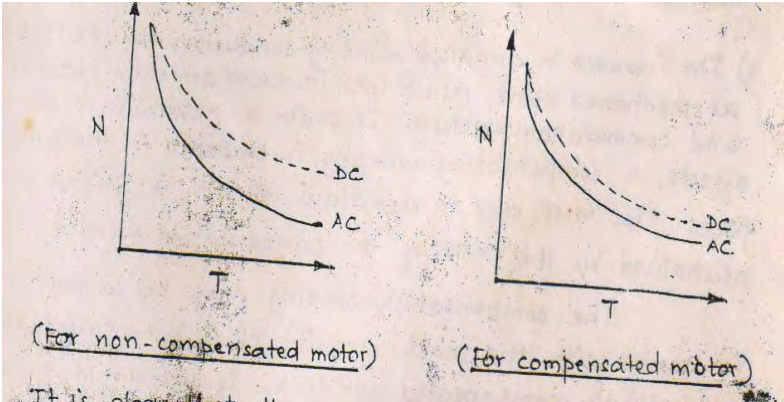


	<p>i) <math>Wt = 0^0, \phi_r = \frac{3}{2} \phi_m</math>      ii) <math>Wt = 60^0, \phi_r = \frac{3}{2} \phi_m</math>      iii) <math>Wt = 120^0, \phi_r = \frac{3}{2} \phi_m</math></p> <p>From the above vector diagrams at different phase angles particularly at <math>0^0</math>, <math>60^0</math> and <math>120^0</math> referred in waveform diagram, it is clear that the resultant flux vector is not stationary but it rotates with <math>N_s</math> ----- (1 Mark)</p>
b)	<p><b>A 3(1), 50 Hz, 4 pole, I.M. has a slip of 4% Calculate:</b>  <b>1) Speed of motor   2) Frequency of rotor emf if the rotor has a resistance of <math>1\Omega</math> and standstill reactance of <math>4\Omega</math>. Calculate the rotor power factor at   i) standstill</b>  <b>ii) a speed of 1440 rpm</b></p>
Ans:	<p>Given Data: 3 ph, 4-pole, 50Hz</p> $N_s = \frac{120 f}{P}$ <p style="text-align: right;">.....(1/2 Mark)</p> $= \frac{120 \times 50}{4}$ $N_s = \frac{120 \times 50}{4} = 1500 \text{ RPM}$ $N = (1 - S) 1500$ $0.04$ $N = (1 - 0.04) 1500$ $N = 1440 \text{ RPM} \dots\dots\dots(1/2 \text{ Mark})$ <p>Frequency of Rotor = <math>S \cdot f</math>.....(1/2 Mark)</p> $= 0.04 \times 50$ <p style="text-align: center;"><b>Frequency of Rotor = 2.0 Hz ..... (1/2 Mark)</b></p> <p><b>i) Power factor at stand still i.e s=1</b></p> $\text{Cos}\phi_2 = \frac{R_2}{\sqrt{(R_2)^2 + (S)^2 \times X_2^2}} \dots\dots\dots(1/2 \text{ Mark})$ $\text{Cos}\phi_2 = \frac{1}{\sqrt{(1)^2 + (4)^2}}$ $\text{Cos}\phi_2 = 0.2425 \text{ lag} \dots\dots\dots(1/2 \text{ Mark})$ <p><b>ii) Power factor at speed of 1440 RPM i.e at s= 0.04 :</b></p> $\text{Cos}\phi_2 = \frac{R_2}{\sqrt{(R_2)^2 + (S)^2 \times X_2^2}} \dots\dots\dots(1/2 \text{ Mark})$ $\text{Cos}\phi_2 = \frac{1}{\sqrt{(1)^2 + (0.04)^2 (4)^2}}$ $\text{Cos}\phi_2 = 0.9874 \text{ lag} \dots\dots\dots(1/2 \text{ Mark})$



<b>c)</b>	<b>Explain the factors which affect the terminal voltage of alternator.</b>
Ans:	<p><b>The factors affecting terminal voltage of alternator: (1 Mark each point)</b></p> <p>The terminal voltage of alternator depends upon: (Any four point are expected)</p> <ol style="list-style-type: none"> <li>1) Load current</li> <li>2) Armature resistance per phase</li> <li>3) Leakage reactance per phase</li> <li>4) Armature reaction reactance per phase</li> <li>5) Excitation (field current)</li> <li>6) Speed</li> <li>7) Load power factor <b>OR</b> when load power factor is unity or lagging, the terminal voltage drops with increase in load, when the load power factor is leading, the terminal voltage increase with increase in load</li> </ol>
<b>d)</b>	<b>A 12 pole, 3-ph, alternator is coupled to an engine running at 500 rpm. It supplies an induction motor which has full load speed of 1440 rpm. Find the slip and the no. of poles of the induction motor.</b>
Ans:	<p>The frequency of generated emf of 3-phase alternator:</p> $f = \frac{N_s \times P}{120} \quad (1 \text{ Mark})$ $f = \frac{(500) \times (12)}{120}$ $f = 50\text{Hz} \dots\dots\dots (1/2 \text{ Mark})$ <p>Let, <math>N_s</math>= Synchronous Speed of I.M close to actual Speed of 1440 RPM:  <math>N_s = 1500 \text{ RPM}</math></p> $P = \frac{(120) (f)}{N_s} \dots\dots\dots (1 \text{ Mark})$ $= \frac{120 \times 50}{1500}$ $P = 4 \text{ Pole} \dots\dots\dots (1/2 \text{ Mark})$ $\% \text{ Slip} = \frac{N_s - N}{N_s} \times 100 \quad (1/2 \text{ Mark})$ $= \frac{1500 - 1440}{1500}$ $\% \text{ Slip} = 0.04 \text{ or } 4 \% \dots\dots\dots (1/2 \text{ Mark})$



e)	<p><b>What is an universal motor? Comment briefly on its constructional features and speed-torque characteristics. Mention it's any two applications.</b></p>
Ans:	<p><b>Diagram of Universal Motor:</b>  <span style="color: red;">(Meaning: 1 Mark. Comments of construction feature:1 Mark, Speed torque characteristics :1 Mark and Application: 1 Mark)</span></p> <p><b>Universal Motor :</b> ..... <span style="color: red;">(1 Mark)</span>          Motors that can be used with a single phase AC source as well as a DC source of supply voltages are called "UNIVERSAL MOTORS"</p> <p><b>Comments on Constructional features:</b> ..... <span style="color: red;">(1 Mark)</span></p> <div style="text-align: center;">  <p><b>OR Equivalent figure</b></p> <ul style="list-style-type: none"> <li>➤ The field core is to be constructed of a material having low hysteresis loss and it is to be laminated to reduce eddy current loss.</li> <li>➤ The field winding is to be designed for smaller number of turns. This helps in reducing the reactance of the field winding.</li> <li>➤ The compensating winding may be connected in series with the motor circuit.</li> </ul> </div> <p><b>Speed-torque characteristics:</b> ..... <span style="color: red;">(1 Mark)</span></p> <div style="text-align: center;">  <p><span style="margin-right: 100px;">(For non-compensated motor)</span> <span>(For compensated motor)</span></p> <p><b>OR Equivalent figure</b></p> </div>





**Comments:**

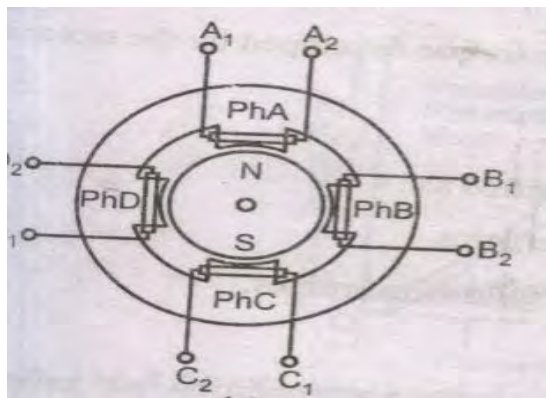
As torque increases speed decreases, the characteristics is similar with DC series motor.

**Application of Universal Motor: ( Any Two application expected) .(1 Mark)**

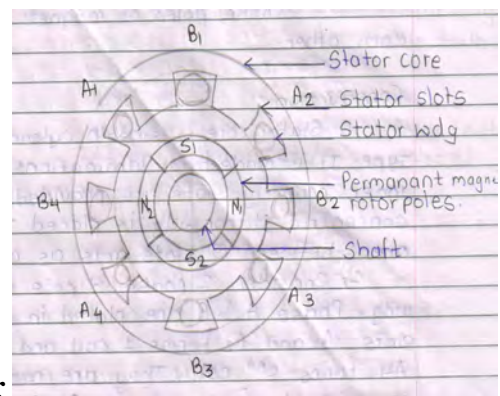
- 1) Mixer
- 2) Food processor
- 3) Heavy duty machine tools
- 4) Grinder
- 5) Vacuum cleaners
- 6) Refrigerators
- 7) Driving sewing machines
- 8) Electric Shavers
- 9) Hair dryers
- 10) Small Fans
- 11) Cloth washing machine
- 12) portable tools like blowers, drilling machine, polishers etc

f) **Explain the working principle of permanent magnet stepper motor**

Ans: **Permanent Magnet Stepper Motor:- ( Figure 2 Mark & Working 2 Mark)**



or

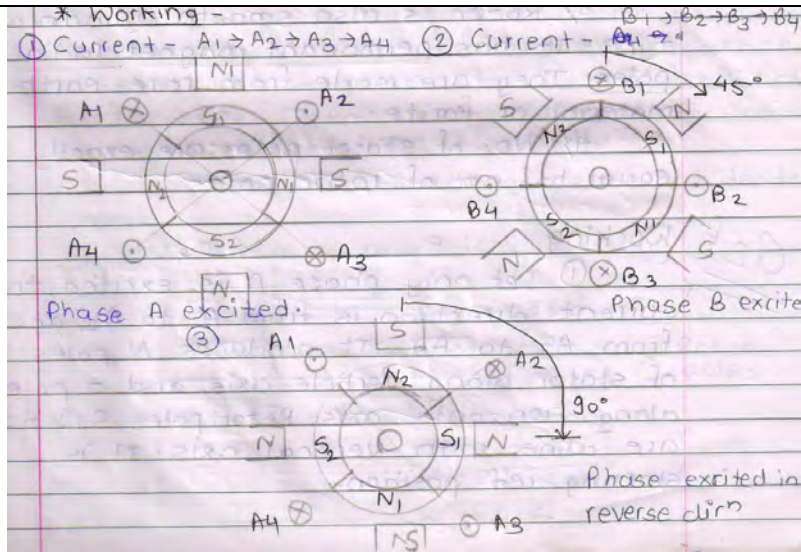


**Working :-**

If the phase is excited in ABCD, due to electromagnetic torque is developed by interaction between the magnetic field set up by exciting winding and permanent magnet. Rotor will be driven in clockwise direction. OR

Working principle: unlike poles attract each other.

**OR**



**OR Equivalent dia.**

**Working :**

- Let only phase A is excited, the current direction is from A1 to A2 and from A3 to A4. It produces N poles of stator along vertical axis, and S pole along horizontal axis. Rotor poles S1 & S2 are aligned with vertical axis. It is starting rest position.
- Now coil  $\phi$  A is switched off & phase B is excited. The current direction is B1 to B2 & B3 to B4. The stator N poles shift in clockwise direction by  $45^\circ$ . Therefore Rotor poles S1 & S2 also rotate by  $45^\circ$  in clockwise direction.
- Now phase B is turned off and Phase A is excited in reverse direction. (A2-A1 & A4-A3) It causes shifted of stator N poles in clockwise direction by  $45^\circ$  again. Hence Rotor poles S1 and S2 also rotate further in clockwise direction by  $45^\circ$
- If switching sequence is maintained as A(+)  $\rightarrow$  B(+)  $\rightarrow$  A (-)  $\rightarrow$  B (-)  $\rightarrow$  A (+) then motor will continuously rotate in clockwise direction.
- The direction of rotation can be reversed by changing switching sequence. If switching sequence is A (+)  $\rightarrow$  B (-)  $\rightarrow$  B (+)  $\rightarrow$  A (-)  $\rightarrow$  A (+) then motor will rotate in anticlockwise direction.
- The number of switching per second decides speed.

**Q.3** Attempt any four of the following : **16 Marks**

a) **Derive torque equation of 3 phase induction motor.**

Ans: **Torque equation of Three phase induction motor at any value of slip:**

Torque of 3-phase induction motor under running condition is directly proportional to the product of working flux per pole, rotor current under running and P.f. of motor circuit under running.

$$\therefore T \propto \phi I_R \cos \phi_R \dots \dots \dots 1$$

**(1 Mark)**



	<p>Now, <math>I_R</math> = Rotor current under running / ph</p> $= \frac{E_r}{Z_r} = \frac{\text{Rotor induced Emf / ph under running}}{\text{Rotor impedance / ph under running}}$ $= \frac{S E_2}{\sqrt{R_2^2 + S^2 X^2}}$ <p>Where, <math>S</math> = Slip      <math>R_2</math> = Rotor resistance / ph    <b>(1 Mark)</b>  <math>X_2</math> = Standstill rotor reactance / ph  <math>E_2</math> = Standstill Rotor induced Emf / ph</p> $\cos \phi_r = \frac{R_2}{Z_r} = \frac{R_2}{\sqrt{R_2^2 + S^2 X^2}} \quad \text{--- (1 Mark)}$ <p>Putting Value of <math>I_r</math> and <math>\cos \phi_r</math> in equation.....1 of Torque</p> $T \propto \phi \left[ \frac{S E_2}{\sqrt{R_2^2 + S^2 X^2}} \right] \left[ \frac{R_2}{\sqrt{R_2^2 + S^2 X^2}} \right]$ $\propto \frac{\phi S E_2 R_2}{R_2^2 + S^2 X^2}$ $T = \frac{K \phi S E_2 R_2}{R_2^2 + S^2 X^2} \quad \text{--- (1 Mark)}$ <p>Where, K= proportionality constant</p>
b)	<p><b>A 12 pole, 50 Hz, 3 phase induction motor has rotor resistance of 0.15 Ω and standstill reactance of 0.25Ωper phase. On full load, it is running at a speed of 480 rpm. The rotor induced emf per phase at standstill is observed to be 32 V. Calculate:</b></p> <p><b>1)Starting torque    2)Full load torque    3)Maximum torque</b>  <b>4) Speed at maximum torque.</b></p>
Ans:	<p>Given Data:  <math>P = 12</math> , <math>f = 50</math> Hz, <math>R_2 = 0.15</math> ohm, <math>X_2 = 0.25</math> ohm, <math>N_{FL} = 480</math> rp., <math>E_2 = 32</math>V</p> <p>i) We have,</p> $N_s = \frac{120 f}{P} = \frac{120 \times 50}{12} = 500 \text{rpm}$ $N_s \text{ in r.p.s.} = \frac{N_s}{60} = \frac{500}{60} = 8.33 \text{ r.p.s (D}_s\text{)} \text{----- (1/2 Marks)}$



ii) Starting Torque: We have

$$T_{\text{Starting}} = \frac{C \cdot R_2}{R_2^2 + X_2^2} \dots\dots\dots (1/2 \text{ Mark})$$

Where,

$$C = \frac{3}{2 \pi N_s} \times E_2^2$$

$$\therefore T_{\text{st}} = \frac{3}{2 \pi \times 8.33} \times \frac{(32)^2 \times 0.15}{(0.15)^2 + (0.25)^2}$$

$$\therefore T_{\text{st}} = 103.53 \text{ N - M}$$

iii) Full load Torque at full load:

$$S = \frac{NS - N}{N} \dots\dots\dots (1/2 \text{ Mark})$$

$$= \frac{500 - 480}{500} = 0.04$$

$$T_{\text{FL}} = \frac{C \cdot S_{\text{FL}} \cdot R_2}{R_2^2 + S_{\text{FL}}^2 X_2^2}$$

$$T_{\text{FL}} = \frac{3}{2 \pi \times 8.33} \times \frac{(0.04) \times (32)^2 \times 0.15}{(0.15)^2 + (0.04 \times 0.25)^2}$$

$$T_{\text{FL}} = 15.58 \text{ N - M} \dots\dots\dots \text{(II)} \dots\dots\dots (1/2 \text{ Marks})$$

iv) Maximum Torque:

$$T_{\text{max}} = \frac{C}{2 + X_2} \dots\dots\dots (1/2 \text{ Mark})$$

$$C = \frac{3}{2 \pi D_s} \times \frac{E_2^2}{2 X_2}$$

$$\therefore T_{\text{max}} = \frac{3}{2 \pi \times 8.33} \times \frac{(32)^2}{2 + (0.25)}$$

$$\therefore T_{\text{max}} = 117.38 \text{ N - M} \dots\dots\dots \text{(III)} \dots\dots\dots (1/2 \text{ Marks})$$



	<p>v) The maximum torque occurs at a Slip:</p> $S_m = \frac{R_2}{X_2}$ <p style="text-align: right;">..... (1/2 Mark)</p> <p>i.e at <math>S_m = \frac{0.15}{0.25} = 0.6</math></p> <p>∴ Speed at Maximum torque</p> $\therefore N = (1 - S_m) N_s \quad \text{----- (IV) ----- (1/2 Marks)}$ $\therefore N = (1 - 0.6) \times 500$ $N = 200 \text{ rpm.}$
c)	<p><b>A 16 pole, 3 phase star connected alternator armature has 12 slots with 24 conductors per slot and the flux per pole is 0.1 Wb. sinusoidally distributed. Calculate the line emf generated at 50 Hz.</b></p>
Ans:	<p>3Ph, Star connected, 16 pole, 50 Hz, alternator</p> $E / \text{ph} = 4.44 \phi f T K_c K_d \text{----- (1/2 Marks)}$ <p>m= Number of slots/Pole/phase</p> $m = \frac{12}{16 \times 3} = 0.25$ $\beta = \frac{180^\circ \text{ Elec.}}{\text{Pole pitch}} \quad \text{(1/2 Marks)}$ <p>Where pole pitch = <math>\frac{\text{No.of Slots}}{\text{Pole}} = \frac{12}{16} = 0.75</math>-----</p> $\beta = \frac{180^\circ \text{ Elec.}}{0.75}$ <p><math>\beta = 240^\circ</math> Elect Considering Full pitched winding ∴ <math>K_c = 1</math></p> $K_d = \frac{\text{Sin } (m \beta / 2)}{m \text{ Sin } (\beta / 2)} \text{----- (1/2 Marks)}$ $K_d = \frac{\text{Sin } [(0.25) (240 / 2)]}{0.25 [\text{Sin } (240 / 2)]}$ $K_d = 0.2165$ <p><math>\phi = 0.1 \text{ Wb} \text{ -- given}</math></p>



	$Z/ph = \frac{\text{Total number of conductors in series}}{3} \text{ -----(1/2 Marks)}$ $Z/ph = \frac{24 \times 12}{3}$ $Z/ph = 96$ <p>Number of turns in series per phase : <math>T/ph = \frac{Z/ph}{2} = \frac{96}{2}</math></p> $T/ph = 48$ $E/ph = 4.44 \phi f T K_c K_d \text{ ----- (1/2 Marks)}$ $E/ph = 4.44(0.1)(50)(48)(1)(0.2165)$ $E/ph = 230.7 \text{ volts ----- (1/2 Marks)}$ $E_{\text{line}} = \sqrt{3} \times E_{ph} \text{ ----- (1/2 Marks)}$ $E_{\text{line}} = 399.59 \text{ volts ----- (1/2 Marks)}$
d)	<b>Derive the emf equation of alternator.</b>
Ans:	<p><b>EMF Equation of alternator:</b></p> <p>Let, P = no. of rotor poles. <math>\phi</math> = Flux per pole      Z= Number of stator conductors</p> <p>N = Speed in rpm</p> $\therefore \text{turns per phase } (T_{ph}) = \frac{Z_{ph}}{2}$ <p><math>\therefore</math> Frequency of induced emf is</p> <p>f = Cycles per rotation x rotation per sec</p> $\therefore = \frac{P}{2} \times \frac{N}{60}$ $\therefore f = \frac{PN}{120} \text{ ----- (1/2 Marks)}$ <p>Consider one rotation of rotor then change in flux linkage is,</p> $d\phi = P \cdot \phi$ <p>Time required for one rotation is,</p> $\therefore dt = \frac{1}{n} = \frac{1}{(N/60)} = \frac{60}{N} \text{ -----Sec. ----- (1 Marks)}$ <p>By faradays law of Electromagnetic induction</p>



$$\therefore \text{Average emf per conductor} = \frac{d\phi}{dt}$$

$$\therefore E_{\text{ave}} / \text{Conductor} = \frac{P \cdot \phi}{(N/60)}$$

$$\therefore E_{\text{ave}} / \text{Conductor} = \frac{P \times \phi \times N}{60} \text{----- Volt-----} \textbf{(1/2 Marks)}$$

$$\therefore E_{\text{ave}} / \text{turn} = 2 E_{\text{ave}} / \text{Conductor} \frac{P \times \phi \times N}{60} \text{----- Volt}$$

$$\therefore E_{\text{ave}} / \text{turn} = 2 \frac{P \times \phi \times N}{60} \text{----- Volt}$$

$$\therefore = \frac{4P\phi N}{120} \text{----- Volt}$$

$$\therefore = 4 \left( \frac{PN}{120} \right) \phi$$

$$\therefore E_{\text{ave}} / \text{turn} = 4 f \phi \quad \therefore \left( f = \frac{PN}{120} \right)$$

$$\therefore E_{\text{ave}} / \text{Phs} = E_{\text{ave}} / \times \text{Number of turns per phase} \\ = 4 f \phi \times T_{\text{ph}} \text{-----} \textbf{(1/2 Marks)}$$

RMS Value per phase is given by,

$$E_{\text{ph}} = E_{\text{ph}} (\text{ave}) \times \text{Form Factor} \\ = 4 f \phi \times T_{\text{ph}} \times 1.11 \text{-----} \textbf{(1 Marks)}$$

$$E_{\text{ph}} = 4.44 \phi \cdot f \cdot T_{\text{ph}} \text{ volts}$$

It is for full pitched concentrated winding. If winding is distributed & short pitched then

$$E_{\text{ph}} = 4.44 \phi \cdot f \cdot T_{\text{ph}} \cdot k_d \cdot k_c \text{ volts}$$

----- **(1/2 Marks)**

Where,  $k_c$  = coil span factor or chording factor

$k_d$  = Distribution factor



e)	<b>Why a single phase induction motor doesn't have a self starting torque? Explain the double revolving field theory.</b>
Ans:	<p><b>Reason for single phase induction motor doesn't have a self starting torque: (2 Mark)</b></p> <ul style="list-style-type: none"> <li>➤ <math>T_f = K \cdot I_2^2 \cdot R_2 / S</math></li> <li>➤ <math>T_B = -K I_2^2 R_2 / (2-S)</math> At Start <math>S = 1</math> <math>T_f = -T_b</math> hence starting torque = 0 hence motor doesn't have a self starting torque</li> </ul> <p style="text-align: center;"><b>OR</b></p> <ul style="list-style-type: none"> <li>➤ When single phase AC supply is given to main winding it produces alternating flux.</li> <li>➤ According to double field revolving theory, alternating flux can be represented by two opposite rotating flux of half magnitude.</li> <li>➤ These oppositely rotating flux induce current in rotor &amp; there interaction produces two opposite torque hence the net torque is Zero and the rotor remains standstill.</li> <li>➤ Hence Single-phase induction motor is not self starting. <b>OR</b></li> </ul> <p>When single phase A.C supply is applied across the single phase stator winding, an alternating field is produced. The axis of this field is stationary in horizontal direction. The alternating field will induce an emf in the rotor conductors by transformer action. Since the rotor has closed circuit, current will flow through the rotor conductors. Due to induced emf and current in the rotor conductors the force experienced by the upper conductors of the rotor will be downward and the force experienced by the lower conductors of the rotor will be upward .The two sets of force will cancel each other and the rotor will experience no torque .Therefore single phase motors are not self starting.</p> <ul style="list-style-type: none"> <li>➤ <b>Double field revolving theory: ----- (2Mark)</b></li> </ul> <div data-bbox="516 1423 1377 1864" data-label="Diagram"> </div> <ul style="list-style-type: none"> <li>➤ Consider two components of flux namely <math>\phi_1</math> &amp; <math>\phi_2</math> each having equal</li> </ul>





magnitude  $\phi_1 = \phi_2 = \phi_M / 2$  it is constant.

- Let, at  $\phi = 0^\circ$  two components are at  $180^\circ$  displaced from each other. Let  $\phi_1$  is along +ve X-axis. Therefore total flux is  $\phi_1 = \phi_2 = \phi_M = 0$
- Let  $\phi_1$  is rotation in anticlockwise direction &  $\phi_2$  in clockwise direction. Both have constant angular speed of  $\omega$  rad/sec.
- At  $\phi = 90^\circ$ ,  $\phi_1$  &  $\phi_2$  rotate by  $90^\circ$  & both align along +ve y-axis. Therefore, total flux  $\phi = \phi_1 = \phi_2 = \phi_M$
- At  $\phi = 180^\circ$ , both fluxes rotate by  $180^\circ$ ,  $\phi_1$  is now along -ve X-axis &  $\phi_2$  is along +ve X-axis. Therefore, total flux is zero
- At  $\phi = 270^\circ$ ,  $\phi_1$  &  $\phi_2$  align with -ve axis & therefore, total flux becomes  $-\phi_M$
- At  $\phi = 360^\circ$ ,  $\phi_1$  is along +ve X-axis &  $\phi_2$  is along -ve X-axis. Therefore, total flux is zero. **OR**

When single phase AC supply is given to main winding it produces alternating flux.

According to double field revolving theory, alternating flux can be represented by two opposite rotating flux of half magnitude.

These oppositely rotating flux induce current in rotor & their interaction produces two opposite torque hence the net torque is Zero and the rotor remains standstill.

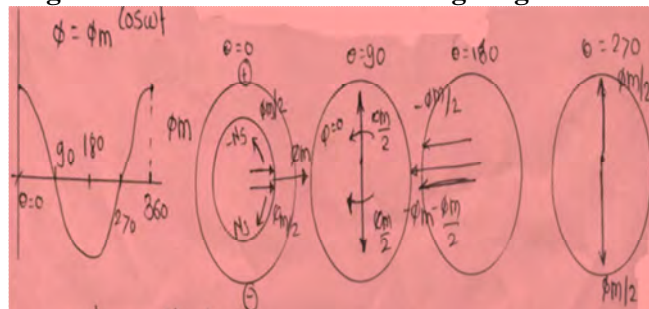
If the rotor rotates in the direction of forward revolving field then, torque in that direction will increase and torque in opposite direction will decrease this will make rotor to rotate in forward direction.

**OR**

When single phase supply is applied across the single phase stator winding, an alternating field is produced. The axis of this field is stationary in horizontal direction. The alternating field will induce an emf in the rotor conductors by transformer action. Since the rotor has closed circuit, current will flow through the rotor conductors.

Due to induced emf and current in the rotor conductors the force experienced by the upper conductors of the rotor will be downward and the force experienced by the lower conductors of the rotor will be upward. The two sets of force will cancel each other and the rotor will experience no torque.

**Production of rotating field with the help of two oppositely rotating fluxes each of half magnitude is shown in the following diagram**



or Equivalent fig.



<b>Q.4 A)</b>	<b>Attempt any three of the following :</b>	<b>12 Marks</b>
a)	<p><b>A 500 V, 3 ph, 50 Hz induction motor develops an output of 15 kW at 950 rpm. If the input power factor is 0.86 lagging. Mechanical losses are 730 W and the stator losses 1500 W. Find</b></p> <p><b>1)The slip 2)The rotor copper loss 3)The motor input</b></p> <p><b>4) The line current.</b></p>	
Ans:	<p><b>Given Data:</b>          3Ph, 50 Hz I.M      Motor o/p = <math>15 \times 10^3</math> W      N = Actual Speed= 950RPM          Assuming , <math>N_s = 1000</math> RPM which is very close with N</p> <p><b>1) The Slip :</b>      <math>\% \text{ Slip} = \frac{N_s - N}{N_s} \times 100 = \frac{1000 - 950}{1000}</math></p> <p style="text-align: right;"><math>\% \text{ Slip} = 0.05</math> or 5 % ----- <b>(1 /2Marks)</b></p> <p><b>Now,</b></p> <p><b>Gross Rotor output</b> = Net Motor output + Mechanical Losses          = (15000+730) watt          = 15730 Watts ----- <b>(1/2 Marks)</b></p> <p><b>2) Rotor Copper Losses</b> = <math>\frac{S}{(1-S)}</math> (Gross Rotor output)      <b>(1/2 Marks)</b></p> <p style="text-align: center;">= <math>\frac{0.05}{(1-0.05)} \times 15730</math>          = 827.895 watts</p> <p style="text-align: right;">Rotor Copper Losses <math>\cong</math> 827.9 Watts ----- <b>(1/2 Marks)</b></p> <p><b>3) Net Motor input:</b></p> <p style="text-align: right;"><b>Rotor Input</b> = <math>\frac{\text{Rotor Copper losses}}{S}</math>      <b>(1/2 Marks)</b></p> <p style="text-align: center;"><b>Rotor Input</b> = <math>\frac{827.895}{0.05}</math>  <b>Rotor Input</b> = 16557.92 Watts</p> <p><b>Net Motor input</b> = Rotor Input + (Stator Losses)          Net Motor input = (16557.92 +1500) Watts</p> <p style="text-align: right;"><b>Net Motor input</b> = <b>18057.92 Watts</b> ----- <b>(1/2 Marks)</b></p> <p style="text-align: center;">Net Motor input = <math>\sqrt{3} V_L I_L \text{ Cos}\phi</math></p>	



WINTER– 2014 Examinations

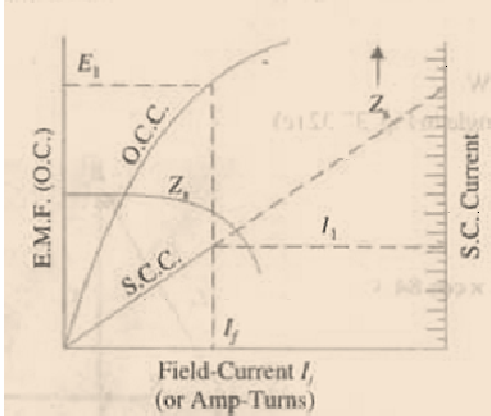
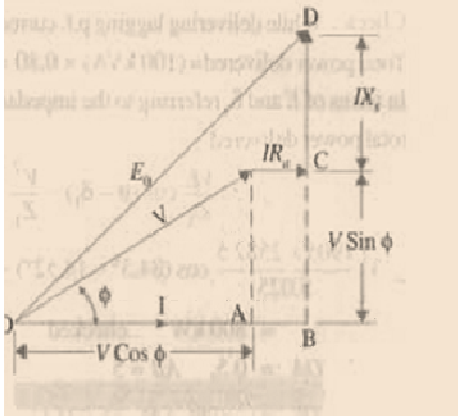
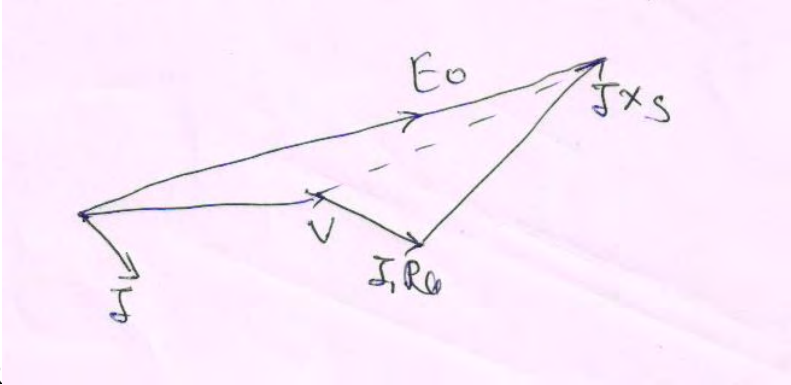
Subject Code: 17511

Model Answer

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	<p><b>4) Line Current of Motor :</b></p> $= \frac{\text{Net motor input}}{\sqrt{3} V_L \cos\phi} \quad \text{(1/2 Marks)}$ $= \frac{18057.92}{\sqrt{3} \times 50 \times 0.86}$ $I_L = \frac{18057.92}{\sqrt{3} \times 50 \times 0.86}$ $I_L = 24.245 \text{ A} \text{ ----- (1/2 Marks)}$																				
b)	<p><b>Compare DC motor and induction motor on the basis of construction, size, speed control and applications.</b></p>																				
Ans:	<p><b>(1 Mark each Points)</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 10%;">S.No</th> <th style="width: 15%;">Points</th> <th style="width: 35%;">DC Motor</th> <th style="width: 40%;">Induction Motor</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">1</td> <td><b>Construction</b></td> <td>Complicated &amp; Bulky/ Projected magnetic Poles (Salient) / Armature Winding is of either lap or wave wound type</td> <td>Simple &amp; Robust / Smooth Cylindrical Poles / Rotor is of either squirrel cage or phase wound type (Slip ring type)</td> </tr> <tr> <td style="text-align: center;">2</td> <td><b>Size</b></td> <td>For same HP capacity the size is large &amp; Weight is more</td> <td>For same HP capacity the size is small &amp; Weight is less</td> </tr> <tr> <td style="text-align: center;">3</td> <td><b>Speed Control</b></td> <td>Easy &amp; Cheap</td> <td>Difficult &amp; Costly</td> </tr> <tr> <td style="text-align: center;">4</td> <td><b>Application</b></td> <td>D.C Series motor: for electric traction. Lift, Rolling mills, Hoist, cranes etc DC Shunt Motor: for constant Speed applications, such as line shafts, lathes, vacuum cleaners, compressors etc</td> <td>Squirrel Cage: Speed Applications, centrifugal pump, Lathes, printing, Washing machine, Compressors, large refrigerators, crushers, Boring mills, textile machinery Slip Ring: For variable speed applications e.g: Driving line shafts Lifts. Pumps, generators, winding machine, printing press, elevators, compressors, textile mills, petrochemical inductive, grinding mill etc</td> </tr> </tbody> </table>	S.No	Points	DC Motor	Induction Motor	1	<b>Construction</b>	Complicated & Bulky/ Projected magnetic Poles (Salient) / Armature Winding is of either lap or wave wound type	Simple & Robust / Smooth Cylindrical Poles / Rotor is of either squirrel cage or phase wound type (Slip ring type)	2	<b>Size</b>	For same HP capacity the size is large & Weight is more	For same HP capacity the size is small & Weight is less	3	<b>Speed Control</b>	Easy & Cheap	Difficult & Costly	4	<b>Application</b>	D.C Series motor: for electric traction. Lift, Rolling mills, Hoist, cranes etc DC Shunt Motor: for constant Speed applications, such as line shafts, lathes, vacuum cleaners, compressors etc	Squirrel Cage: Speed Applications, centrifugal pump, Lathes, printing, Washing machine, Compressors, large refrigerators, crushers, Boring mills, textile machinery Slip Ring: For variable speed applications e.g: Driving line shafts Lifts. Pumps, generators, winding machine, printing press, elevators, compressors, textile mills, petrochemical inductive, grinding mill etc
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c)	<p><b>Explain the procedure to calculate voltage regulation of a 3 phase alternator by synchronous impedance method with necessary graphs and phasor diagram. (2 Marks)</b></p>
Ans:	<p style="text-align: right;"><b>(2 Marks)</b></p> <div style="display: flex; justify-content: space-around;">   </div> <p style="text-align: center;">OR</p>  <p style="text-align: center;">OR</p> <p style="text-align: center;"><b>or Equivalent characteristics /Vector dig.</b></p> <p><b>The procedural steps for synchronous impedance method are as follows: (2 Marks)</b></p> <ol style="list-style-type: none"> <li>1) The Open Circuit Characteristics OCC is plotted from open circuit test</li> <li>2) Short Circuit characteristics is plotted from short circuit test: Short circuit characteristics are straight line through origin. Both characteristics plotted for common field current base. Consider field current <math>I_f</math> and the corresponding OC voltage <math>E_1</math>. During short circuit, at the same field current, the whole <math>E_1</math> is being used to circulate the short circuit current (<math>I_{sc}</math>) in armature.</li> <li>3) The synchronous impedance <math>Z_s</math> can be calculated as,  <math display="block">E_1 = I_{sc} Z_s \rightarrow Z_s = \frac{E_{1OCC}}{I_{sc}}</math> </li> <li>4) By performing resistance test, Effective armature resistance, <math>R_a</math> can be calculated Synchronous reactance can be calculated as</li> </ol>



	$X_s = \sqrt{Z_s^2 - R_a^2}$ <p>5) The regulation of the alternator at a particular load condition can be calculated as, the generated EMF; <math>E_0</math> can be calculated as,</p> $E_0 = \sqrt{(V \cos \phi + I_a R_a)^2 + (V \sin \phi + I_a X_s)^2}$ <p>The % regulation = <math>\frac{E_0 - V}{V} \times 100</math></p>
d)	<b>Why is it necessary to run the alternators in parallel?</b>
Ans:	<b>Reason for necessary to run the alternators in parallel:</b> <b>(Any Four point expected; 1 Mark each)</b> <ol style="list-style-type: none"><li><b>1. Continuity in supply system:</b> Continuity in supply system is we have two or more alternator in parallel and if one is out of order then the power supply can be maintained with the help of another alternator.</li><li><b>2. More Efficiency:</b> The alternators can be put ON or cut OFF as per the load demand. The efficiency of alternator is maximum at full load. Therefore we can put ON required number of alternators as per load demand and operate the alternators at full load capacity.</li><li><b>3. Maintenance and repair:</b> With more number of alternators in parallel, anyone can be taken out of maintenance and repair without disturbing the supply. The smaller units are very easily repairable.</li><li><b>4. Standby of reserved unit:</b> In case of number of small alternators in parallel, The standby alternator required is also of small capacity.</li><li><b>5. Future expansion:</b> Considering the probable increasing in demand in future, some additional units are installed and can be connected in parallel.</li><li><b>6. Saving In Fuel:</b> Since almost all alternators are operated on full load no anyone alternator operates lightly loaded.</li></ol> <p style="text-align: center;"><b>OR</b></p> <ol style="list-style-type: none"><li>Several small units connected in parallel are more reliable than a single large unit. If one of small units is disabled, the entire power supply is not cut –off.</li><li>The units may be connected in service and taken out of service to correspond with the load on the station. This keeps the units loaded to their full load capacity &amp; increases the efficiency of the operation.</li><li>Out of several units if one unit fails, it can be repaired easily without the failure of supply to consumers.</li><li>Additional units can be connected in parallel with the resent units to correspond with the growth of the load.</li><li>Cost of the spares if any required for repair, maintenance will be reduced.</li></ol>



<b>Q. 4 B)</b>	<b>Attempt any one of the following :</b>	<b>06 Marks</b>
a)	<b>Define voltage regulation of alternator? On what factors regulation depends? Explain in brief</b>	
Ans:	<b>Voltage Regulation of Alternator:</b> It is defined as the rise in voltage when full load is removed, keeping excitation & speed of alternator constant, expressed as percentage of rated terminal voltage is called “Voltage regulation”. <b>OR</b> It is defined as the ratio of sudden rise or fall in voltage when the load is removed suddenly to the rated terminal voltage, keeping speed & excitation of alternator constant. <b>Following factors on which voltage regulation depends:</b> <b>1. Armature resistance per phase:</b> As armature resistance increases $I_a R_a$ drop increases, which make voltage regulation poor. <b>2. Armature Leakage flux:</b> If leakage flux is more, the leakage reactance $X_L$ increases which increases $I_a X_L$ drop. Hence regulation becomes poor. <b>3. Magnitude of load current:</b> If load current increases $I_a R_a$ and $I_a X_L$ drop increases and armature reaction effect also increases. Therefore terminal voltage drops which makes regulation poor. <b>4. Load Power factor:</b> i) For lagging power factor the effect of armature reaction is demagnetizing and therefore the main flux reduces, considerably which causes poor regulation. ii) For unity P.f, the effect of armature reaction is cross magnetizing, therefore distortion in main flux will be resulted & hence regulation is comparatively less. iii) For leading P.f, the effect of armature reaction is strong magnetizing therefore main flux will be more stronger and so terminal voltage actually increases which gives negative regulation.	<b>(2 Marks)</b>
b)	<b>O.C. and S.C. test were performed on a 3 phase 0.5 MVA, 3.6 kV, star connected alternator. The results are given below : O.C. : If= 10 A, Vsc = 3000 volt, S.C.: If = 10 A, Isc = 150 A, Ra/ph = 1 Q, Calculate the percentage, regulation for full load condition at 0.8 p.f. lagging.</b>	
Ans:	Given Data: 3Ph, 0.5 MVA, 3.6 KV star connected alternator, $V_T$ Line 3.6 KV ( $V_T/ph= 2078.46$ ) $I_a \text{ line Current} = \frac{\text{MVA} \times 10^6}{(\sqrt{3}) \times (V_{T\text{Line}})}$	<b>(1/2 Marks)</b>



$$I_a \text{ line Current} = \frac{(0.5) \times 10^6}{(\sqrt{3}) \times (3.6) \times 10^3}$$

$$I_a \text{ line Current} = 80.188\text{A} \text{-----}(1/2 \text{ Marks})$$

$$Z_s / \text{Ph} = \frac{\text{O.C. Voltage}}{\text{S.C.Current / ph}} \text{ at } I_f = 10\text{A} \text{-----} (1/2 \text{ Marks})$$

$$Z_s / \text{Ph} = \frac{3000 / \sqrt{3}}{150}$$

$$Z_s / \text{Ph} = 11.547 \ \Omega \text{-----} (1/2 \text{ Marks})$$

$$X_s / \text{Ph} = \sqrt{(Z_s / \text{ph})^2 - (R_a / \text{ph})^2} \quad (1/2 \text{ Marks})$$

$$X_s / \text{Ph} = \sqrt{(11.547)^2 - (1)^2}$$

$$X_s / \text{Ph} = 11.504 \ \Omega \text{-----} (1/2 \text{ Marks})$$

Now,

**% Regulation at full load for 0.8 Lagging P.f :**

$$E / \text{ph} = \sqrt{(V_T \cos\phi + I_a R_a)^2 + (V_T \sin\phi + I_a X_s)^2} \quad (1 \text{ Marks})$$

$$E / \text{ph} = \sqrt{[(2078.46)(0.8) + (80.188)(1)]^2 + [(2078.46)(0.6) + (80.188)(11.504)]^2}$$

$$E / \text{ph} = 2782.96 \text{-----} (1/2 \text{ Marks})$$

$$\% \text{ Regulation} = \frac{E_o / \text{ph} - V_T / \text{ph}}{V_T / \text{ph}} \times 100 \text{-----} (1 \text{ Marks})$$

$$\% \text{ Regulation} = \frac{2782.96 - 2078.46}{2078.46} \times 100$$

$$\% \text{ Regulation} = 33.895 \% \text{-----} (1/2 \text{ Marks})$$

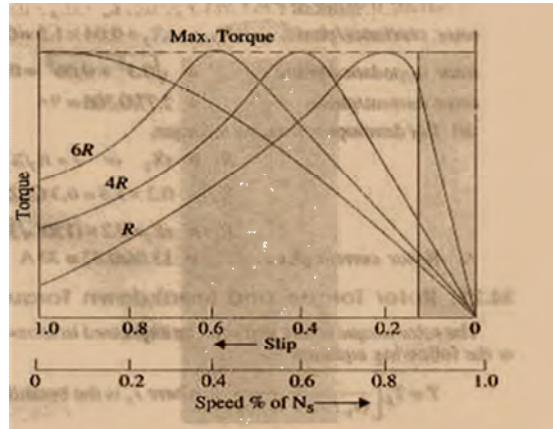


<b>Q.5</b>	<b>Attempt any four of the following :</b>	<b>16 Marks</b>
a)	<b>A 20 HP, three phase, 50 Hz, 4 pole induction motor has a full load slip of 4%. The friction and Windage losses are 500 watts; calculate the rotor copper loss and rotor speed.</b>	
Ans:	<p>Given data: 3-ph, 4 Pole, 50 Hz, 20 HP I.M, <math>S_f = \text{full load slip} = 4\%</math></p> <p>Net output of Motor = 20 HP  <math>= (20 \times 735.5) \text{ watts}</math>  <math>= 14710 \text{ watts}</math> ----- <b>(1/2 Marks)</b></p> <p>Gross Rotor output = Net Motor output + Mechanical Losses-----<b>(1/2 Marks)</b>  <math>= 14710 + 500 \text{ watts}</math>  <math>= 15210 \text{ watts}</math> ----- <b>(1/2 Marks)</b></p> <p><b>Rotor Copper Losses</b> = <math>\frac{S}{(1-S)}</math> (Gross Rotor output) ----- <b>(1 Marks)</b>  <math>= \frac{0.04}{(1-0.04)} \times 15210</math>  <math>= 633.75 \text{ watts}</math>----- <b>(1 /2Marks)</b></p> <p><b>Rotor Speed (N)</b> = <math>(1-S)N_s</math> where <math>N_s = \frac{120 f}{P} =</math> <b>(1/2 Marks)</b>  <math>\frac{120 \times 50}{4} = 1500 \text{ RPM}</math>  <math>N = (1-0.04) \times 1500</math>  <b>Motor Speed N = 1440 RPM</b> ----- <b>(1/2 Marks)</b></p>	
b)	<b>Describe with the help of curves the effect of variation of a rotor circuit resistance on the torque-slip characteristics of an induction motor.</b>	
Ans:	<b>( Explanation of Effect- 2 Marks Characteristics -2 Marks)</b>	
	<p><b>Explanation: From the below characteristics:-</b></p> <ul style="list-style-type: none"> <li>➤ When rotor resistance increases, maximum torque condition occurs at higher values of slip and characteristics shifts towards left hand side.</li> </ul> <p>The maximum torque condition can be obtained at any required slip by changing rotor resistance.</p>	





**Figure:**



or characteristics

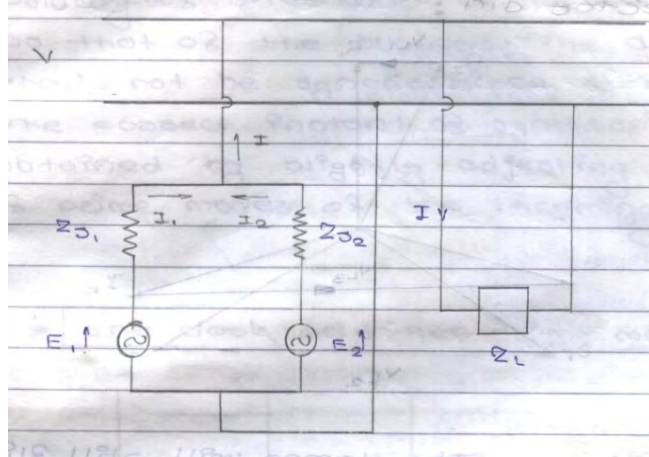
c) Explain the concept of load sharing.

Ans:

( NOTE: Student may give answer either by Derivation or without derivation any one should be considered)

**Figure :**

(Figure: 2 Mark & Explanation: 2 Mark)



**Explanation:**

Consider two machines with identical Speed load characteristics running in a parallel with a common terminal voltage of  $V$  volts and load impedance  $Z_L$

Let the generated e.m.f of the two machine 1 and 2 operating in parallel be  $E_1$  and  $E_2$  respectively and synchronous impedances per phase be  $Z_{S1}$  and  $Z_{S2}$  respectively

$$1) I = I_1 + I_2$$

$$2) E_1 = V + I_1 Z_{S1}$$

$$E_1 = I \times Z_L + I_1 \times Z_{S1}$$

$$E_1 = (I_1 + I_2) Z_L + I_1 \times Z_{S1}$$

$$E_1 = I_1 (Z_L + Z_{S1}) + I_2 \times Z_L \text{-----} I$$



	<p style="text-align: center;">3) <math>E_2 = V + I_2 \times Z_{S2}</math>  <math>E_2 = I \times Z_L + I_2 \times Z_{S2}</math>  <math>E_2 = (I_1 + I_2) Z_L + I_2 \times Z_{S2}</math>  <math>E_2 = I_2 (Z_L + Z_{S2}) + I_1 \times Z_L</math>-----II</p> <p>From equation I and II :-</p> <p style="text-align: center;"><math>\therefore I_1 = \frac{(E_1 - E_2) Z_L + E_1 \times Z_{S2}}{(Z_{S1} + Z_{S2}) Z_L + Z_{S1} \times Z_{S2}}</math>  <math>\therefore I_2 = \frac{(E_2 - E_1) Z_L + E_2 \times Z_{S1}}{(Z_{S1} + Z_{S2}) Z_L + Z_{S1} \times Z_{S2}}</math>  <math>\therefore I = I_1 + I_2 \quad \text{and} \quad V = I \times Z_L</math></p> <p><b>Note:</b> - If the two alternators are at No-load. <math>I_c</math> equal to No-Load circulating current, Therefore</p> $I_c = \frac{E_1 - E_2}{Z_{S1} - Z_{S2}}$ <p><b>Load Shifting:</b></p> <p style="text-align: center;">The load shifting from running alternator to the incoming alternator</p> <ul style="list-style-type: none"> <li>➤ By increasing the mechanical power input to the prime mover of the incoming alternator.</li> <li>➤ &amp; simultaneously reducing the mechanical power input to the prime-mover of the existing alternator.</li> </ul> <p><b>Note:-</b></p> <p style="text-align: center;">Load can't be shifted from one machine to the another by adjustment of excitation. The excitation changes voltage &amp; power factor of the alternator.</p>
d)	<p><b>A total load of 1200 kW is shared equally by two identical alternators at 6000 volts and 0.866 lagging p.f. The current of one alternator is 70 A at lagging p.f. Find the p.f. of both the alternators. Both alternators are 3 phase star connected.</b></p>
Ans:	<p><b>Solution:</b> Total load: 1200 kW, Voltage: 6000V, P.f: 0.866 lag current of all = 70 A</p> <p><b>Step 1: Total active load (KW<sub>L</sub>) = 1200 kW</b></p> <p><b>Step 2 : Total reactive load :</b></p> <p style="text-align: center;"><math>\therefore \phi = \cos^{-1} (0.866) = 30^\circ \text{ Elec.}</math></p> <p style="text-align: center;"><math>\therefore \text{Total reactive load} = 1200 \text{ kW} \times \tan 30</math></p> <p style="text-align: center;"><math>\therefore \text{Total reactiv load} = 692.8203 \text{ KVAR}</math> ----- <b>(1/2 Marks)</b></p>



**Step 3: Reactive Power shared by alternator 1:**

$$\therefore = P_1 \tan \phi_1 \text{----- (1/2 Marks)}$$

$$\therefore P_1 = \sqrt{3} V_L \times I_L \times \cos \phi$$

$$\therefore \phi_1 = \cos^{-1} \left[ \frac{P}{\sqrt{3} \times V_L \times I_L} \right] \text{----- (1/2 Marks)}$$

$$\therefore \phi_1 = \cos^{-1} \left[ \frac{600 \times 10^3}{\sqrt{3} \times 6000 \times 70} \right]$$

$$\therefore \phi_1 = \cos^{-1}(34.431)$$

$$\therefore \cos \phi_1 = 0.8247 \text{ lag ----- (1/2 Marks)}$$

$$\text{Reactive power shared by alternator 1} = 600 \times \tan (34.431)$$

$$= 411.3379 \text{ KVAR ----- (1/2 Marks)}$$

**Step 4: Reactive Power shared by alternator 2 = Total reactive – Reactive power of**

$$\text{alt 1} \quad \quad \quad = 692.8203 - 411.3379$$

$$\text{Reactive Power shared by alternator 2} = 281.4824 \text{ KVAR----- (1/2 Marks)}$$

But,

$$\text{Reactive power shared by alternator 2} = P_1 \tan \phi_2$$

$$281.4824 = 600 \times \tan \phi_2 \text{----- (1/2 Marks)}$$

$$\tan \phi_2 = \frac{281.4824}{600}$$

$$\tan \phi_2 = 0.4691$$

$$\phi_2 = \tan^{-1} (0.4691)$$

$$\phi_2 = 25.1331^\circ$$

$$\cos \phi_2 = 0.9053^\circ \text{----- (1/2 Marks)}$$



OR student may write this way

**Step 1: Total active load (KW<sub>L</sub>) = 1200 kW is shared equally by two indicate alternators 1 & 2**

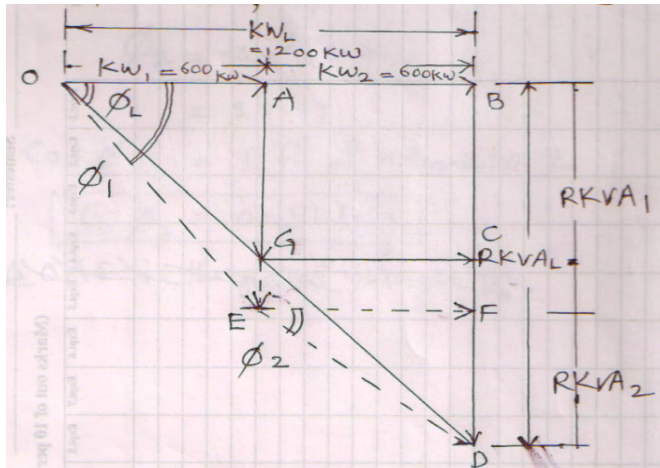


figure is not compulsory

➤ The load current shared alternator 1 =  $I_1 = 70$  Amp

$$\therefore \cos \phi_1 = \frac{KW_1}{\sqrt{3} V_T I_1} \text{----- (1/2 Marks)}$$

$$\therefore \cos \phi_1 = \frac{600 \times 10^3}{\sqrt{3} \times 6000 \times 70}$$

$\therefore$  Power factor alternator  $\cos \phi_1 = 0.825$  lag ----- (1/2 Marks)

$$\therefore \phi_1 = \cos^{-1} (0.825) = 34.43^\circ \text{ Elec. ----- (1/2 Marks)}$$

$$\therefore \text{length } (l)' AE' = l (BF) = l(OA) \tan \phi_1 .$$

$$\therefore RKVA_1 \text{ of alternator 1} = 600 kW \times \tan 34.43$$

$$\therefore RKVA_1 = 411.3 \text{ RKVA ----- (1/2 Marks)}$$

$$\therefore \text{length } (l)' BD' = KVA \text{ of load} = l(OB) \tan \phi_L .$$

$$\therefore \phi_L = \cos^{-1} (0.866) = 30^\circ \text{ Elec.}$$

$$\therefore RKVA_L = 1200 kW \times \tan 30$$

$$\therefore RKVA_L = 692.82 \text{ RKVA ----- (1/2 Marks)}$$

$$\therefore RKVA \text{ of alternator} = l (FD) = l (BD) - l (BF) = 692.82 - 411.3$$

$$\therefore RKVA_2 = 281.52 \text{ ----- (1/2 Marks)}$$



**RA Δ EFD is the power triangle of alternator No.2:**

$$\therefore \tan \phi_2 = \frac{l(FD)}{l(EF)} = 0.47 \text{ ----- (1/2 Marks)}$$

$$\therefore \phi_2 = \tan^{-1} (0.47)$$

$$\therefore \phi_2 = 25.17$$

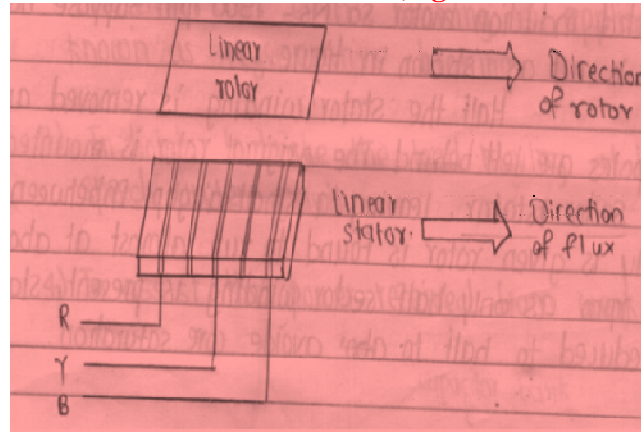
$$\therefore \cos \phi_2 = P.f. \text{ of alternator 2}$$

$$\therefore \text{Power factor alternator } \cos \phi_2 = 0.91 \text{ lag ----- (1/2 Marks)}$$

e) **Explain the principle of operation of linear induction motor.**

Ans:

**(Figure- 2 Marks & Principle – 2 Marks)**



or Equivalent fig.

➤ **Principle of operation linear induction motor:-**

In a sector IM, if sector is made flat and squirrel cage winding is brought to it we get linear I.M. In practice instead of a flat squirrel cage winding, aluminum or copper or iron plate is used as rotor.

The flat stator produces a flux that moves in a straight line from its one end to other at a linear synchronous speed given by  $V_s = 2 \omega f$

Where,  $V_s$  = linear synchronous speed in m/sec

$\omega$  = width of one pitch in m.

$f$  = supply frequency (Hz)

The speed does not depends on number of poles but only on the poles pitch and supply frequency. As the flux move linearly it drags the rotor plate along with it in same direction. However in much practical application the rotor is stationary while stator moves.



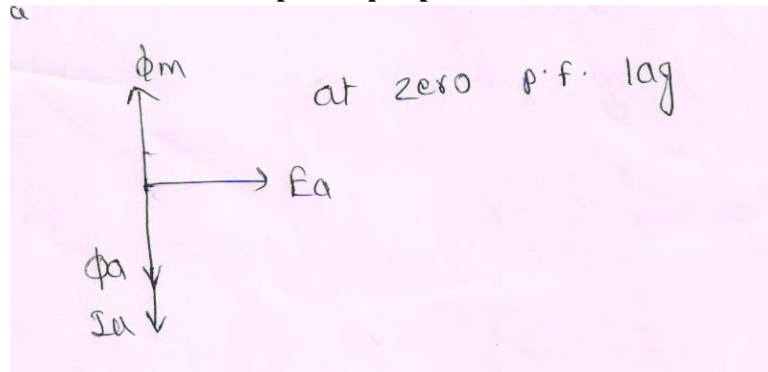
f)	<b>What is an induction generator? State its principle of operation</b>
Ans:	<p><b>Induction generator:</b> <span style="float: right;"><b>(2 Mark)</b></span></p> <p>When rotor of induction motor runs faster than synchronous speed, induction motor runs as generator and called as induction generator. It converts mechanical energy it receives from the shaft into electrical energy which is released by stator. However, for creating its own magnetic field, it absorbs reactive power <math>Q</math> from the line to which it is connected. The reactive power is supplied by a capacitor bank connected at the induction generator output terminals.</p> <p><b>Figure:-</b> <span style="float: right;"><b>(Figure- 1 Marks &amp; Principle – 1 Marks)</b></span></p> <div data-bbox="483 825 1235 1260" data-label="Diagram"></div> <p style="text-align: center;"><b>or Equivalent fig.</b></p> <p>➤ <b>The principle of operation induction Generator:</b></p> <p>When rotor of induction motor runs faster than synchronous speed (<math>N &gt; N_s</math>), induction motor runs as generator and called as induction generator. It converts mechanical energy it receives from the shaft into electrical energy which is released by stator. However, for creating its own magnetic field, it absorbs reactive power <math>Q</math> from the line to which it is connected. The reactive power is supplied by a capacitor bank connected at the induction generator output terminals.</p>



<b>Q.6</b>	<b>Attempt any four of the following :</b>	<b>16 Marks</b>									
a)	<b>State two applications each for the single phase capacitor start capacitor run and shaded pole induction motors.</b>										
Ans:	<table border="1"><thead><tr><th>Sr.No</th><th>Types of 1-Ph Induction Motor</th><th>Applications (Any Two expected)</th></tr></thead><tbody><tr><td>1</td><td>Capacitor Start Capacitor run <b>(Any Two Applications 2Marks)</b></td><td>Fans, Blowers, Grander, Drilling Machine, Washing Machine, Refrigerator, Air conditioner, Domestic Water Pumps,</td></tr><tr><td>2</td><td>Shaded pole motor <b>(Any Two Applications 2Marks)</b></td><td>Recording Instruments, Record Player, Gramophones, toy Motors, Hair dryers, Photo copy machine, Advertizing display</td></tr></tbody></table>		Sr.No	Types of 1-Ph Induction Motor	Applications (Any Two expected)	1	Capacitor Start Capacitor run <b>(Any Two Applications 2Marks)</b>	Fans, Blowers, Grander, Drilling Machine, Washing Machine, Refrigerator, Air conditioner, Domestic Water Pumps,	2	Shaded pole motor <b>(Any Two Applications 2Marks)</b>	Recording Instruments, Record Player, Gramophones, toy Motors, Hair dryers, Photo copy machine, Advertizing display
Sr.No	Types of 1-Ph Induction Motor	Applications (Any Two expected)									
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2	Shaded pole motor <b>(Any Two Applications 2Marks)</b>	Recording Instruments, Record Player, Gramophones, toy Motors, Hair dryers, Photo copy machine, Advertizing display									
b)	<b>State the four applications of induction generators.</b>										
Ans:	<b>Applications:- Any Four</b>	<b>(Each Application : 1 Mark)</b>									
	1. It is used in wind mills. 2. It is used to assist the power received from weak transmission lines in the remote areas. 3. To compensate reactive power from the supply. 4. Regenerative breaking of hoists driven by the three phase induction motors 5.with energy recovery systems in industrial processes										
c)	<b>What is armature reaction? Discuss the effect of lagging p.f. on armature reaction.</b>										
Ans:	<b>Armature Reaction: -</b> When the armature conductors carry current they produce their own flux this flux affects the main pole flux. Due to the change in flux the terminal voltage available at the load conditions will be different. The effect of armature flux on pole flux is called as armature reaction.	<b>(2 Mark)</b>									



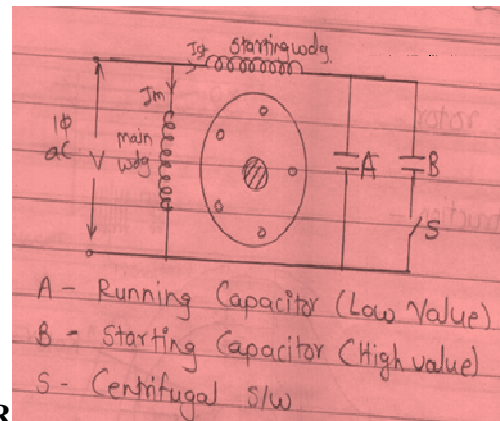
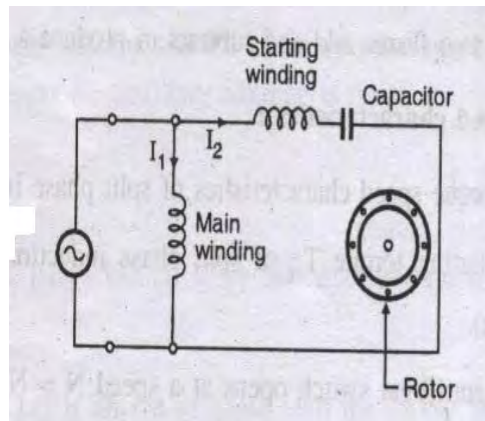
The effect of armature reaction depends upon power factor the load:



**For lagging P.f. or inductive load:** - In this case the armature flux opposes the main flux. This effect is called as **de-magnetizing Effect**. Due to this, the main flux will be weakened and terminal voltage drops i.e.  $V_T < E$  .....-(2 Mark)

d) Explain the role of capacitor in a single phase capacitor start capacitor run induction motor

(Figure -2 Mark & Explanation -2 Mark)



Ans:

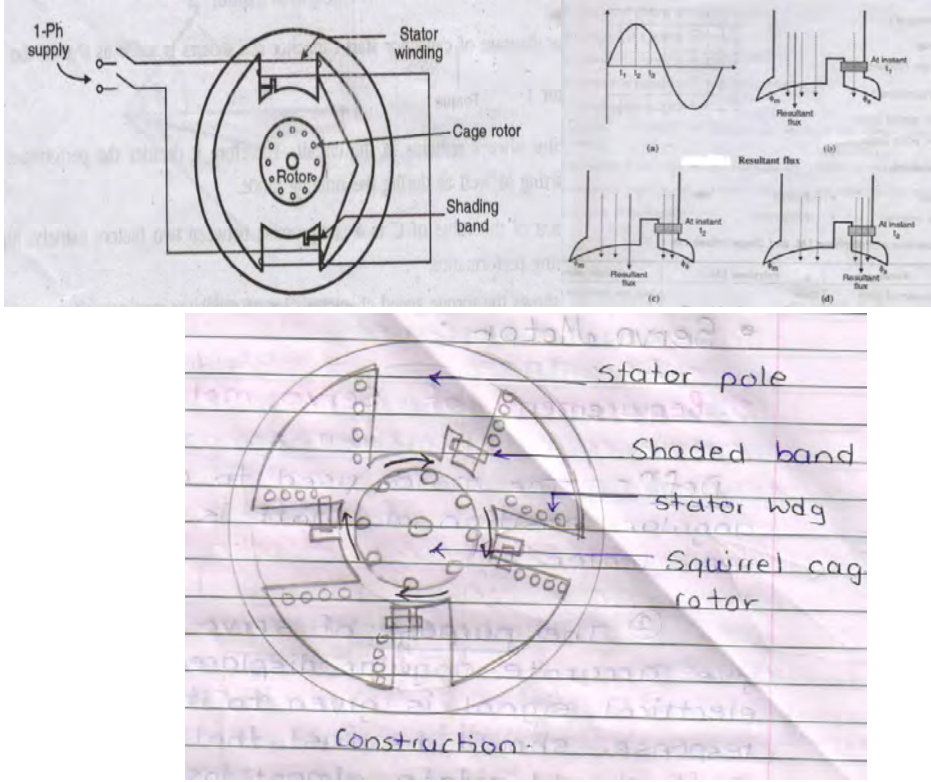
OR  
or Equivalent fig

In these motors one capacitor is connected in series with the auxiliary winding. There is no centrifugal switch. Thus this winding along with the capacitor remains energized for both starting and running conditions. **Capacitor used serves the purpose of obtaining necessary phase displacement at the time of starting and also improves the power factor of the motor.**

Due to capacitor motor operation becomes salient





e)	<p><b>With neat schematic diagram, briefly explain the principle of operation of a shaded pole single phase induction motor.</b></p>
Ans:	<p><b>i) Shaded Pole Induction Motor :</b> <span style="color: red;">(Figure-2 Mark &amp; Explanation: 2 Mark)</span></p>  <p><b>Equivalent Fig.</b></p> <p><b>Correct diagram of pole axis shifting from left to right</b></p> <p><b>Working:-</b></p> <p>When single phase supply is applied across the stator winding an alternating field is created. The flux distribution is non uniform due to shading coils on the poles.</p> <p>Now consider three different instants of time <math>t_1, t_2, t_3</math> of the flux wave to examine the effect of shading coil as shown in the fig above. The magnetic neutral axis shifts from left to right in every half cycle, from non shaded area of pole to the shaded area of the pole. This gives to some extent a rotating field effect which may be sufficient to provide starting torque to squirrel cage rotor.</p>