

Winter-2016 Examinations

Subject Code: 17511

Model Answer

Page 1 of 40

Important suggestions to examiners:

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more importance. (Not applicable for subject English and communication skills)
- 4) While assessing figures, examiner may give credit for principle components indicated in a figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
- 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and model answer.
- 6) In case some questions credit may be given by judgment on part of examiner of relevant answer based on candidate understands.
- 7) For programming language papers, credit may be given to any other program based on equivalent concept.

Q.1 (A)	Attemp	t any THREE:	12 Marks
a)	Compare squirrel cage induction motor & slip ring induction motor. (Any four points).		
Ans:	(Any Four point expected: Each Point -1 Mark)		
	S.No.	Squirrel Cage Induction Motor	Slip Ring Induction Motor
	1	Rotor is in the form of bars	Rotor is in the form of 3-ph winding
	2	No slip-ring and brushes	Slip-ring and brushes are present
	3	External resistance cannot be connected	External resistance can be connected
	4	Small or moderate starting torque	High Starting torque
	5	Starting torque is fixed	Starting torque can be adjust
	6	Simple construction	Completed construction
	7	High efficiency	Low efficiency
	8	Less cost	More cost
	9	Less maintenance	Frequent maintenance due to slip-ring and brushes.
	10	Starting power factor is poor and power factor on running is better	Starting power factor is adjustable & large but low power factor on full load
	11	Size is compact for same HP	Relatively size is larger
	12	Speed control by stator control method only	Speed can be control by stator & rotor control method



	Winter-2016 Examinations			
Subje	ct Code: 17511 <u>Model Answer</u> Page 2 of 40			
b)	State why three phase Induction Motor never run on synchronous speed.			
Ans:	(4 Marks)			
	The working principle of three phase induction motor is based on relative motion			
	between rotating magnetic field and rotor conductors i.e. (Ns - N), According to Lenz's law			
	rotor will try to catch the synchronous speed of rotating magnetic field to oppose the 'cau			
	producing it'. But rotor never succeeds due to frictional losses.			
	If rotor catches the synchronous speed of rotating magnetic field, $(N_s - N)$ i.e relative			
	motion will be zero and rotor stops to rotate and therefore three phase induction motor can			
	never run on synchronous speed.			
c)	Explain with diagram how star-delta starters are used for reducing the starting current of 3			
Ans:	phase induction motors. Reason for star-delta starters are used for reducing the starting current of 3 phase induction			
7 115.	motors. (Wiring Diagram-2 Mark & Explaination-2 Mark)			
	> At Starting the stator winding is connected in star connection			
	At the time of starting in star connection, $Iph = \frac{Vph}{Z_{sc}}$ and $Vph = \frac{V_L}{\sqrt{3}}$			
	Therefore starting current controlled to a safe value because if reduced stator			
	voltage			
	> After the motor has reaches nearly steady state speed, the change over switch is			
	thrown to connect motor in delta			
	Diagram of Star -Delta starters:			







Winter- 2016 Examinations Model Answer

Page 4 of 40

	4. As the high frequency harmonics are illuminated, Hysteresis & eddy current losses will be		
	reduced and this increases the efficiency.		
Q.1 (B)	Attempt any ONE: 6 Marks		
a)	Explain speed control method of 3 phase Induction motor by the follow (i) Frequency control (ii) Stator voltage control (iii) Rotor resistance control (iii)	ing methods. ontrol	
Ans:	i) By varying applied Frequency (Frequency control): (2 Mark)		
	> The synchronous speed of an induction motor is given by N_s	$f = \frac{120 \times f}{P}$.	
	 It is clear from the equation that the speed of the induction motor can be changed by changing the frequency of the supply. 		
	ii) Stator Voltage Control (by varying applied voltage):	(2 Mark)	
	This method is very easy but rarely used in commercial practice because a large variation of voltage produces a very small change in speed and much energy is wasted.		
	In this method three resistances are inserted in series with the stator winding of the motor and the value of these resistances is varied by a common handle, so that equal resistances come in the stator circuit.		
	 For a particular load when voltage increases, speed of the mot and vice-versa. 	tor also increases	
	iii) Rotor resistance control (by rotor rheostatic control:	(2 Mark)	
	MAN SWICH I 2 3 ROTOR RESISTANCE		
	 In this method star connected external resistances (of continue 	ous rating) are	
	connected in the rotor circuit.		
	\succ The speed of the motor increases with the decrease of resistant	ce in the rotor	
	circuit.		
	> The change in speed is approximately inversely proportional t	to the external	







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Winter– 2016 Examinations <u>Model Answer</u>

Page 6 of 40





Winter-2016 Examinations **Model Answer** Subject Code: 17511 Page 7 of 40 (Figure: 2 Mark) Power input to stator from Rotor input]_ Air-gap power Mechanical power power Pa developed, Pm 1 mains Power at rotor shaft Psh Stator Stator Rotor Rotor Friction Windage I²R core loss 12R core loss loss at loss loss (negligible bearings at small slips) and slip rings (if any) loss OR Rotoz 48035 Net Net Rotoz moto Input Motoz Stator losses Rotoż Cu losses 0/p Mech 0/p Input BHP J3VTILGS 2TTNT 735-2 Power stages of 3 ph. I.M. OR Input to motor Rotor input Stator copper and iron losses Rotor output or Mechanical power developed Rotor copper losses Rotor output Windage and friction losses 10 BHP Derive relation for rotor copper loss. Consider 3-ph induction motor: (2 Mark) Gross rotor output = $2 \pi N Tg$ Where, N in rps & T_g in N-m

If rotor rotates with synchronous speed, there will not be copper losses in rotor and

hence rotor output will be equal rotor input







	Winter-2016 Examinations	
Subje	ct Code: 17511 <u>Model Answer</u>	Page 9 of 40
	The torque equation of induction motor is given by: $T = \frac{K \phi S E_2 R_2}{R_2^2 + S^2 X^2}$	
	The simplified form of the above torque equation- $T \propto S \times V^2$ (:: $\phi \propto F$ and $F \propto F$ and $F \propto V$)	
	 From the above equation it is clear that the torque at any speed is p square of supply voltage V. Hence any change in supply voltage will be having great effect on 	roportional to the running torque and
	 maximum torque. As supply voltage decreases up to 50 % of the rated value, maximu decreases almost up to 50 % of maximum torque. This effect is shown in the above torque-speed characteristics 	ım torque
c)	A 12 pole, 30, alternator is couple to an engine running at 500 rp induction motor which has full load speed of 1440 rpm. Find the s poles of the induction motor.	om. It supplies an lip and the no. of
Ans:	The frequency of generated emf of 3-phase alternator: $f = \frac{N_s \times P}{120}$ $f = \frac{(500) \times (12)}{120}$	(1 Mark)
	120 f = 50Hz Let, N _S = Synchronous Speed of I.M close to actual Speed of 1440 RPM: N _s = 1500 RPM	(1/2 Mark)
	$P = \frac{(120) (f)}{N_s}$ = $\frac{120 \times 50}{1500}$	(1 Mark)
	P = 4 Pole	(1 /2Mark)
	% Slip = $\frac{N_s - N}{N_s} \times 100$ = $\frac{1500 - 1440}{1500}$	(1/2 Mark)
	% Slip = 0.04 or 4 %	.(1/2 Mark)



Subje	Winter- 2016 Examinationsct Code: 17511Model AnswerPage 10 of 40			
d)	Explain the factors which affect the terminal voltage of alternator.			
Ans:	(Any Four Foster superted, 1 Mark each point)			
	(Any Four Factor expected: 1 Mark each point)			
	The terminal voltage of alternator depends upon: (Any four point are expected)			
	1) Load current			
	2) Armature resistance per phase			
	3) Leakage reactance per phase			
	4) Armature reaction reactance per phase			
	5) Excitation (field current)			
	6) Speed			
	7) Load power factor OR when load power factor is unity or lagging, the terminal voltage drops with increase in load, when the load power factor is leading, the terminal voltage increase with increase in load			
e)	A motor is to be operated from 230 V, 50 Hz single phase AC and 220 V DC supply. Identify above motor and describe its working with neat sketch.			
Ans:	Name of Motor :(1 Mark)			
	➤ A motor is operated from 230 V, 50 Hz single phase A.C. and 220 V D.C. supply i.e.			
	motor operates on both AC and DC supply this motor is called as a: Universal			
	Motor			
	Working principle with neat sketch: -(Figure : 2 Mark & Working : 1 Mark)			
	Main Field Wdg.			





		Winter- 2016 Examinati	ons	
Subje	ct Code: 17511	Model Answer	Page 13 of 40	
	> The direction of	of rotation of the rotor can be reve	rsed by reversing the phase difference,	
	from leading to	b lagging (or vice versa) between	the control phase voltage and the	
	reference phas	e voltage.		
	-	OR		
	The a.c. servomotor is basically consists of a stator and a rotor. The stator carries two windings, uniformly distributed and displaced by 90° in space, from each other.			
	One winding is called as main winding or fixed winding or reference winding . The reference winding is excited by a constant voltage a.c. supply.			
	Control voltage form servoamplifier	A.C. supply 000 Reference winding Rotor	The other winding is called as control winding. It is excited by variable control voltage, which is obtained from a servoamplifier. The windings are 90° away from each other and control voltage is 90° out of phase with respect to the voltage applied to the reference winding. This is necessary to obtain rotating magnetic field. The schematic stator is	
	Wi	nding	shown in the Fig. 9.20.	
	Fig. 9.20 3	Stator of a.c. servomotor	To reduce the loading on the	
	i.e. the impedance of	the control winding is increased by	amplifier, the input impedance	
	with the control wind	ling.	using a turning capacitor in paraner	
Q.3	Attempt any Four :		16 Marks	
a)	Derive the condition	for T _{max} . of a 3 phase inductio	n motor.	
Ans:		ote: The student can follow for	different method of derivation also	
	Let us consider the e	quation of torque,		
		$T = \frac{K \phi S E_2 R_2}{R^2 + S^2 K^2}$		
		$\pi_2 + \delta \Lambda$	(1 Mark)	
	Condition of	maximum torque can be found of	but by taking derivative of torque	
	equation w.r.t. Slip ar	nd equating it to zero. For the sin	nplicity of derivation, let us put $\frac{1}{T} = M$	
		$M = \frac{R_2^2 + S^2 X_2^2}{2}$		
		$\overline{K \phi S E_2 R_2}$	(1 Mark)	

	Winter-2016 Examinations	
Subje	ct Code: 17511 <u>Model Answer</u>	Page 14 of 40
	$M = \frac{R_2^2}{K \phi S E_2 R_2} + \frac{S^2 X_2^2}{K \phi S E_2 R_2}$ $R_2 \qquad S X^2$	
	$M = \frac{K_2}{K \phi S E_2} + \frac{S R}{K \phi E_2 R_2}$	
	$\frac{d(M)}{dS} = \frac{d}{dS} \left[\frac{R_2}{K \phi S E_2} + \frac{S X_2^2}{K \phi E_2 R_2} \right] = 0$	(1 Mark)
	$-\frac{R_2}{K \phi S^2 E_2} + \frac{X_2^2}{K \phi E_2 R_2} = 0$	
	$\frac{X_2^2}{K\phi FR} = \frac{R_2}{K\phi S^2 F}$	
	$\begin{array}{cccc} \mathbf{X} \psi & \mathbf{L}_2 & \mathbf{X}_2 & \mathbf{X} \psi & \mathbf{S} & \mathbf{L}_2 \\ \mathbf{S}^2 \mathbf{X}_2 & \mathbf{R}_2^2 & \mathbf{R}_2^2 \end{array}$	
	$\frac{1}{K\phi E_2 R_2} = \frac{1}{K\phi S^2 E_2}$	
	$S^2 X_2^2 = R_2^2$	
	$\ldots \mathbf{K}_2 = \mathbf{S} \mathbf{X}_2$	
	This is the condition for maximum torque of 3-Ph induction	motor under running
b)	A 3 phase, 6 pole 50 Hz induction motor has a slip of 1% at no load load. Determine (i) synchronous speed (ii) no load speed (iii) full (iv) frequency of rotor at standstill (v) frequency of rotor current a	d, and 3% at full load speed at full load
Ans:	Given Data: Full load Slip = 3% No load Slip = 1% Pole = 6 , F = 50 Hz	z V = 400 volt
	i) Synchronous speed = $120 f$	
	$Ns = \frac{1}{P}$	(1/2 Mark)
	$Ns = \frac{120 \times 50}{6}$	
	Ns = 1000 RPM	
		(1/2 Mark)
	ii) No Load Speed N = $(1-S)(N_S)$	(1/2 Mark)
	=990 <i>RPM</i>	(1/2 Mark)
	iii) Full Load Speed N = $(1-S)(N_s)$	· · · · ·

Winter-2016 Examinations Subject Code: 17511 **Model Answer** Page 15 of 40 =(1-0.03)(1000)=970 *RPM* ----- (1/2 Mark) iv) The frequency of rotor at standstill: Slip at standstill 1 : $f_1 = Sf$ ------ (1/2 Mark) $f_1 = (1) \ge 50$ $f_1 = 50 Hz$ ------ (1/2 Mark) v) frequency of rotor current at full load: $f^1 = S f$ $f^1 = (0.03) \times 50$ $f^1 = 1.5 Hz$ ------ (1/2 Mark) Describe the concept of synchronous impedance. Also define the term leakage c) reactance, armature reaction reactance with respect to an alternator. Ans: 1) Synchronous impedance: (2 Mark) It is a fictitious impedance employed to account for the voltage effects in armature circuit produced by the actual armature resistance, the actual armature leakage reactance, and the change in air gap flux produced by armature reaction. OR $Z_{\rm S} = R_{\rm a} + j \left(X_{\rm L} + X_{\rm a} \right)$ $= R_a + j (X_s)$ Where. Z_S = synchronous impedance, R_a = Armarure resistance, X_L = Leakage reactance, X_a = Armature reaction reactance, X_S = Synchronous reactance 2) Leakage reactance: (1 Mark) The working flux does not only passes through intended path. Some part of working flux will be lost due to leakage. Hence leakage reactance is defined as the factor or parameters which represents the leakageflux OR When armature carries a current, it produces its own flux. Some part of this flux completes its path through the air around the conductors itself. Such a flux is called

		Winter- 2016 Examinations	
Subje	ect Code: 17511	Model Answer	Page 16 of 40
	leakage flux. The reactance	equivalent reactance due to this leakage	e flux is called as ;leakage
	3) Armature Reacti The eff	on reactance: - ect of armature flux on main flux is ca	(1 Mark) lled as armature reaction and the
	parameter which r	epresents the armature reaction at variou	us power factor or load condition,
	is called armature	reaction reactance	
d) Ans:	A 3-phase 50 Hz, conductors per slo the phase and line 3-Ph, Star connected	& pole alternator has a star connecte t. The flux per pole is 0.05 wb, sinus voltages. d, Assuming Pole : 8 Pole, 50 Hz, alter	ed winding with 120 slots and 8 soidally distributed. Determine nator
	Important Note: 7	The data of pole are not given, So the as it is not mentioned, Accordingly the	candidate can assume this data e answer will change
	E/ph = 4	44ø f T Kc Kd	(1/2 Marks)
	$m= Nun$ $m= \frac{12}{8 \times}$ $\beta = \frac{180^{\circ}}{Pole}$ Where po	nber of slots/Pole/phase $\frac{D}{3} = 5$ <u>Elec.</u> <u>pitch</u> le pitch = $\frac{No.of Slots}{Pole} = \frac{12}{8} = 15^{}$	(1/2 Marks)
		$\beta = \frac{180^{\circ} Elec.}{15}$ $\beta = 12^{\circ} Elect$	
	Considering Full pit	ched winding $\therefore K_{\rm C} = 1$	
	$K_d = \frac{S}{n}$	$\frac{\ln (m \beta/2)}{\ln \sin (\beta/2)}$	(1/2 Marks)
	$K_{d} = \frac{S}{(5)}$ $K_{d} = \frac{C}{0.5}$	$\frac{in [(5) (12/2)]}{[Sin (12/2)]}$ $\frac{0.5}{5226}$	

	Winter-2016 Examinations	
Subje	ct Code: 17511 <u>Model Answer</u>	Page 17 of 40
	$K_d = 0.9567 \qquad \qquad$	(1/2 Marks)
	$Z/ph = \frac{\text{Total number of conductors in series}}{3}$	(1/2 Marks)
	$Z/ph = \frac{120 \times 8}{3}$ $Z/ph = 320$	
	Number of turns in series per phase: $T/ph = \frac{Z/ph}{2} = \frac{320}{2}$ T/ph = 160	
	$E/ph = 4.44\phi f T Kc Kd$	(1/2 Marks)
	E / ph = 4.44(0.05) (50) (160) (1) (0.9567)	
	$E / ph = 1699.09 \ volts$	(1/2 Marks)
	E line = $\sqrt{3} \times \text{Eph}$	
	<i>E line</i> = 2942.93 <i>volts</i>	(1 /2Marks)
e)	Describe with phasor diagrams phase splitting technique in or induction motor.	capacitor start run
Ans:	Phasor diagrams phase splitting technique in capacitor start run in (Phasor Diagram : 2 Mark & Expla	duction motor: nation : 2 Mark)
	$I_{S}(\phi_{S})$	
	Vollage	
	(Øm) or equivalent	figure

	Winter-2016 Examinations	
Subje	ect Code: 17511 <u>Model Answer</u>	Page 18 of 40
	Explanation:	(2 Mark)
	\succ I _m - the current passing through main winding having inductive	nature, lags behind
	voltage axis by @ 90 [°] Elec. This sets up the a.c flux Φ_m	
	\blacktriangleright I _s - the current passing through the starting winding circuit cons	isting capacitors,
	Leads the voltage axis by some angle. This sets up the a.c flux	Φ_s
	> Both the fluxes Φ_m and Φ_s are of a.c nature, working in same	air gap & having a
	phase difference. The interaction between these two fluxes Φ_{μ}	$_{n}$ and Φ_{s} sets up the
	resultant one flux which is of rotating nature	
	Rotating magnetic field is the basic requirement of I.M for self-	-starting, thus by using
	split phase principle technique in capacitor start run induction i	notor can be made
	self-starting characteristics.	
$\mathbf{O}(\mathbf{A})$	Attomations TWO	12 Marks
Q.4 (A)	Attempt any TwO:	$\frac{12 \text{ IVIarks}}{12 \text{ IVIarks}}$
a)	ohm at standstill. Full load torque is obtained at 360 rpm. Calcula maximum torque occurs (b) the ratio of maximum to full load to resistance per phase to be inserted in the rotor circuit to get starting.	te. (a) Speed at which rque. (c) The external maximum torque at
Ans:	Given Data:	
	3-Ph Pole = 16, $F = 50 \text{ Hz}$, 746 K.W I.M, Speed at full lo	ad torque = 360 rpm
	$Z_{s}/Ph = (R_{2} + j X_{2}/ph)$	
	$Z_{s}/Ph = (0.02 + j 0.15) \ \Omega/ph$	
	i) Synchronous speed =	
	$Ns = \frac{120 f}{R}$	
	<i>F</i> 120×50	(1/2 Mark)
	$N_S = \frac{1}{16}$	
	Ns = 375 RPM	(1/2 Mark)
	ii) The maximum torque occurs at the condition:	
	$\mathbf{R}_2 = S \left(X_2 \right) \qquad - \qquad$	(1/2 Mark)

	Winter-2016 Examinations	
Subject Code: 17511	Model Answer	Page 19 of 40
	$S = R_2$	
	$S = \frac{1}{X_2}$	
	s 0.02 0.122	
	$S = \frac{1}{0.15} = 0.133$	
	<i>S</i> = 0.133	
		(1/2 Mark)
iii) Speed at S	Slip = 0.133	
	$\mathbf{N} = N_s \ (1 - S)$	
	= (375) (1.0.133)	
	N – 325 RPM	
	IV - 525 KI WI	(1/2 Mark)
iv) Full Load S	Slip S _f = $S_f = \frac{(N_s - N)}{N}$	
	(375-360)	
	$S_f = \frac{1}{375}$	
	<i>S</i> _{<i>f</i>} = 0.04	(1/2 Marks)
We have ,		
	T_{max} $a^2 + S_f^2$	
	$\overline{T_{full}} = \overline{2 a S_f} \dots$	(1/2 Mark)
V	Where, $a = R_2 / X_2 = 0.1333$ and $S_f = 0.04$	
	$\frac{T_{\text{max}}}{1} = \frac{(0.1333)^2 + (0.04)^2}{(0.04)^2}$	
	T_{full} 2(0.1333)(0.04)	
	$T_{\rm max}$ _ 0.01937	
	T_{full}^{-} 0.010664	
	T_{max} 1.92	
	$\frac{1.82}{T_{full}} = 1.82$	(1 Mark)
iv) The Maxin	num torque condition at Starting for Slip ring I.M:	:
	$R_2 + r = X_2$ When $S = 1$	
		(1/2 Mark)
r/ph = re	esistance per ph to be connected in series to get maximu	im torque at starting
	$= X_2 - R_2$	
		(1/2 Mark)

	Winter-2016 Examinations	
Subje	ect Code: 17511 <u>Model Answer</u> Pa	nge 20 of 40
	= 0.15 - 0.02	
	$r/ph = 0.13 \Omega \tag{1}$	/2 Mark)
		(2 WIIIK)
b)	Explain how each of the following can reduce starting current of 3 Ph IM.(i) By inserting resistance in rotor winding(ii) By connecting auto transformer in stator winding.	
Ans:		
	i) By inserting resistance in rotor winding can reduce starting current of 3 p	hase IM: (3 Marks)
	This method is only applicable to slip-ring motors. At the instant of star	ting, the
	external rotor resistance can be kept at maximum value. Therefore heavy start	ing current
	can be controlled.	
	ii) By connecting autotransformer in stator winding:	(3 Marks)
	> At the instant of starting, the position of the slider/variable tap is kept a	at zero
	voltage position.	
	> When the slider moves gradually in clockwise direction, the voltage ap	plied to
	three phase induction motor will be increased in steps.	
	➢ At starting reduced voltage can be applied to 3-phase induction motor and hence	
	heavy starting current will be reduced or controlled.	
	When motor start to rotate and achieve about 70 % of the rated speed, voltage can be applied to 3-phase induction motor.	the rated
	Thus by using 3-phase auto transformer as a starter, starting current can be	e controlled.
c)	A 3 ph star connected alternator is rated at 1600 kVA, 13500 V. The armater resistance and synchronous reactance are 1.5 ohm and 30 ohm respectively Calculate percentage regulation for a load of 1280 kW at power factor of (i) 0.8 leading (ii) Unity (iii) 0.8 lag	ure effective y per phase.
Ans:	Solution:-	
	3-Ph, star connected alternator,	
	$V_{\rm T}$ Line = 13.5 x 10 ³ KV $R_a / Ph = 1.5 \Omega$ & $X_s / Ph = 30$	Ω
	$V_T / Ph = 13.5 \times 10^3 / \sqrt{3} = 7794.23$ Volt	
	$I_{a} line Current = \frac{KW \times 10^{3}}{(\sqrt{3}) \times (V_{TLine}) Cos\phi}$	(1/2 Marks)

	Winter– 2016 Examinations	
Subject Code: 17511	Model Answer	Page 21 of 40
I	line Current = $\frac{(1280) \times 10^3}{(\sqrt{3}) \times (13.5) \times 10^3 (0.8)}$	
	$I_a line Current = 68.43 A$	(1/2 Marks)
Now, i) % regulatio	n at 0.8 leading Power Factor;	
E / pł	$h = \sqrt{(V_T \ Cos\phi + I_a R_a)^2 + (V_T \ sin\phi - I_a X_s)^2} - \dots$	(1/2Mark)
E_{ph}	$= \sqrt{(7794.23 \times 0.8) + (68.43 \times 1.5)^2 + (7794.23 \times 0.6)^2}$	$-68.43 \times 30)^2$
	$Eph = \sqrt{6338.25)^2 + (2326.64)^2}$	
	$Eph = \sqrt{45583814.59}$	
	<i>Eph</i> = 6751.5786 <i>Volt</i>	(1/2Mark)
Reg	$gulation = \frac{6751.5786 - 7794.23}{7794.23} \times 100 = -13.38\%$	
% Reg	gulation = - 13.38 %	(1 Mark)
ii) % regulatio	on at Unity Power Factor;	
	$I_a \ line \ Current = \frac{KW \times 10^3}{(\sqrt{3}) \times (V_{TLine}) \ Cos \phi}$	
i i	$I_a line Current = \frac{1280 \times 10^3}{(\sqrt{3}) \times 13500 \times 1}$	
	I_a line Current = 54.74 Amp	
E/p	$bh = \sqrt{\left(V_T \ \cos\phi + I_a R_a\right)^2 + \left(V_T \ \sin\phi + I_a X_s\right)^2}$	
E_{ph}	$=\sqrt{(7794.23 \times 1 + 54.74 \times 1.5)^2 + (7794.23 \times 0 + 54.74 \times 1.5)^2}$	$4 \times 30)^2$
Eph	$a = \sqrt{64733552.6}$	
	<i>Eph</i> = 8045.72 <i>Volt</i>	(1/2 Mark)
Reg	$gulation = \frac{8045.72 - 7794.23}{7794.23} \times 100 = 3.23\%$	
% Reg	gulation = 3.23 %	(1/2Mark)

	Winter-2016 Examinations	
Subje	ct Code: 17511 <u>Model Answer</u>	Page 22 of 40
	iii) % Regulation at 0.8 Lagging Power Factor: $\cos \phi = 0.8$, $\sin \phi = 0.6$	
	$E / ph = \sqrt{(V_T \ Cos\phi + I_a R_a)^2 + (V_T \ sin\phi + I_a X_s)^2} - \dots$	(1/2Mark)
	$E_{ph} = \sqrt{(7794.23 \times 0.8) + (68.43 \times 1.5)^2 + (7794.23 \times 0.6 + 68.43 \times 1.5)^2}$	$\overline{30)^{2}}$
	$E_{ph} = \sqrt{(6235.38) + (102.645)^2 + (4676.54 + 2052.9)^2}$	
	$Eph = \sqrt{(6338.025)^2 + (6729.44)^2}$	
	$Eph = \sqrt{40170560.9 + 45285362.71}$	
	<i>Eph</i> = 9244.2373 <i>Volt</i>	(1/2Mark)
	$\operatorname{Re} gulation = \frac{9244.2373 - 7794.23}{7794.23} \times 100 = 18.60\%$	
	% Regulation = 18.60 %	(1 Mark)
Q.4 (B)	Attempt any ONE:	<u>6 Marks</u>
a)	alternator when the nature of load on the alternator is resistive, purely	y inductive and
	purely capacitive.	
	The effect of armature reaction depends upon power factor the load:	
	1) For Resistive load or unity P.f.:- In this case the armature flux case	rosses the main
	flux. This Effect is called <u>'Cross magnetizing effect</u> . Due to this,	the main flux
	will be distributed and terminal voltage drops ie $V_T \langle E$	(1 Mark)
	2) For lagging P.f. or inductive load: - In this case the armature flu	x opposes the
	main flux. This effect is called as <u>de-magnetizing Effect</u> . Due to	this, the main
	flux will be weakened and terminal voltage drops ie $V_T \langle E $	(1 Mark)
Ans:	3) For leading P.f. or capacitive load: - In this case the armature flue	ux assists the
	main flux. This Effect is called as Strong magnetizing and due to	this, the main
	flux will be stronger & terminal voltage increases ie $V_T \rangle E$	(1 Mark)
	OR Student May write this way	

	Winter-2016 Examinations	
Subject Code: 17511	Model Answer	Page 24 of 40
	I_a line Current = $\frac{(0.5) \times 10^6}{(\sqrt{3}) \times (3.6) \times 10^3}$	
	I_a line Current = 80.188A	(1/2 Marks)
	Z_{s} /Ph = $\frac{O.C. Voltage}{S.C.Current / ph}$ at $I_{F} = 10A$	(1/2 Marks)
	$Z_{\rm s} / {\rm Ph} = \frac{3000 / \sqrt{3}}{150}$	
	Z_{s} /Ph =11.547 Ω	(1/2 Marks)
	$X_{s} / Ph = \sqrt{(Z_{s} / ph)^{2} - (R_{a} / ph)^{2}}$	(1/2 Marks)
	$X_{\rm s}/{\rm Ph} = \sqrt{(11.547)^2 - (1)^2}$	
Now,	X_{s} /Ph =11.504 Ω	(1/2 Marks)
% Regulat	ion at full load for 0.8 Lagging P.f :	
	$E/ph = \sqrt{(V_T \cos\phi + I_a R_a)^2 + (V_T \sin\phi + I_a X_S)^2}$	(1 Marks)
E/ph =	$\sqrt{\left[(2078.46)(0.8) + (80.188)(1)\right]^2 + \left[(2078.46)(0.6) + (80.188)(1)\right]^2}$	80.188)(11.504)] ²
	$\frac{E}{ph} = 2782.96$	(1/2 Marks)
% R	egulation = $\frac{E_0 / ph - V_T / ph}{V_T / ph} \times 100 \cdots$	(1 Marks)
% R	egulation = $\frac{2782.96 - 2078.46}{2078.46} \times 100$	
0/ D		

Winter- 2016 Examinations Model Answer

Page 25 of 40

Q.5	Attempt any FOUR : 16 Marks
	A 3 phase induction motor has a starting torque of 100% and a maximum torque of
a)	(ii) Full load slip (iii) Rotor current at starting in per unit of full load rotor current.
Ans:	Given Data:
	$T_{st} = 1.0$ T_{FL} I
	$T_{\rm max} = 2.0 \qquad T_{FL}$ II
	Solution:
	$\frac{T_{st}}{T_{max}} = \frac{1}{2} = \frac{2 a}{1 + a^2} (Where \ a = \frac{R_2}{X_2})$
	$\frac{T_{st}}{T_{\max}} = 4 \ a = 1 + a^2$
	$\frac{T_{st}}{T_{\max}} = a^2 - 4 a + 1 = 0$
	Solving Quadratic equation :
	$roots = \left(\frac{-b \pm \sqrt{b^2 - 4ac}}{2a}\right)$
	$a = \left(\frac{-(-4) \pm \sqrt{(-4)^2 - 4 \times (1 \times 1)}}{2 \times (1)}\right)$
	$a = (\frac{(4) - \sqrt{16 - 4}}{2})$
	$a = 0.2679$ $(a = \frac{R_2}{X_2} \therefore \frac{R_2}{X_2} = 0.2679)$
	i) The Slip at maximum torque (S _m) = $\frac{R_2}{X_2}$
	$S_m = 0.2679$ (1 Mark)
	$T_{\max} = 2.0$ T_{FL} given
	$\frac{T_{FL}}{T_{\text{max}}} = \frac{1}{2} = \frac{2 a S_f}{a^2 + S_F^2} Where S_F = Full \ load \ Slip$

Subject Code: 17511	Winter– 2016 Examinations <u>Model Answer</u>	Page 26 of 40
	$\frac{T_{FL}}{T_{max}} = \frac{2 \times 0.2679 \times S_f}{(0.2679)^2 + S_f^2} = \frac{1}{2}$	
	$S_f^2 - 1.0716 \ S_f + 0.0676 = 0$	
Solving Quadrat	tic equation :	
ii) Full Load S	Slip :	
$S_f =$	$(\frac{-b \pm \sqrt{b^2 - 4 ac}}{2 a})$	
S _f	$=(\frac{1.0716\pm\sqrt{(1.0716)^2-4\times(0.0676)}}{2})$	
S _f	$=(\frac{1.0716\pm0.93697}{2})$	
S_{f}	- 0.06731	(1 Mark)
(iii) Rotor curren	nt at starting in per unit of full load rot	or current:
	$\alpha K_{1} E_{2} I_{st} \frac{R_{2}}{\sqrt{R_{2}^{2} + X_{2}^{2}}}$. (Where S	=1)
	$I_{st} \alpha I_{st} \frac{R_2}{\sqrt{R_2^2 + X_2^2}} \qquad $	I
	$\alpha I_{FL} \frac{R_2}{\sqrt{R_2^2 + S_f^2 X_2^2}}.$	II
Dividing Equa	tion I by equation II :	
$\frac{T_{st}}{T_{FI}}$	$\frac{R_{2}}{I_{FL}} = \frac{I_{st}}{I_{FL}} \frac{\frac{R_{2}}{\sqrt{R_{2}^{2} + X_{2}^{2}}}}{\frac{R_{2}}{\sqrt{R_{2}^{2} + S_{f}^{2}X_{2}^{2}}}}$	
$rac{T_{st}}{T_{FL}}$	$=\frac{I_{st}}{I_{FL}}\frac{\sqrt{R_2^2+S_f^2X_2^2}}{\sqrt{R_2^2+X_2^2}}$	
Dividing Num	herator and Denominator in square root to	erms by X_2^2

Winter-2016 Examinations		
Subje	ect Code: 17511 <u>Model Answer</u>	Page 27 of 40
	$\frac{T_{st}}{T_{FL}} = \frac{I_{st}}{I_{FL}} \frac{\sqrt{\frac{R_2^2}{X_2^2} + S_f^2}}{\sqrt{\frac{R_2^2}{X_2^2} + 1}}$	(1 Mark)
	$T_{st} = 1.0$ T_{FL} given	
	Putting the value of $\frac{R_2}{X_2} = 0.2669$ and $S_f = 0.06731 in$	above equation
	$1.0 = \frac{I_{st}}{I_{FL}} \sqrt{\frac{(0.2679)^2 + (0.06731)^2}{(0.2679)^2 + 1}}$	
	$\frac{I_{st}}{I_{FL}} = \frac{1.0}{0.2669}$	
	$\frac{I_{st}}{I_{FL}} = 3.746 I_{FL} \qquad$	(1 Mark)
b)	Derive the ratio of full load torque and maximum torque of a 3 p	hase induction motor.
Ans:	The Equation of torque: $T = \frac{S E_2^2 R_2}{R_2^2 + S^2 X_2^2}$	(1/2 Mark)
	\blacktriangleright The torque will be maximum when Slip = R_2/X_2	
	 Substituting the value of this slip in above equation we get the torque as 	e maximum value of
	$T_{\text{max}} = K \frac{E_2^2}{X_2^2} N - m$	(1/2 Mark)
	The equation of the full load torque:	
	$T_{f_{ull}} = \frac{S_f E_2^2 R_2}{R_2^2 + (S_f^2 X_2^2)}$	(1/2 Mark)
	Where, $S_f = Slip$ at full load The ratio full load torque to maximum torque:	

	Winter- 2016 Examinations	
Subje	ct Code: 17511 Model Answer	Page 28 of 40
	$\frac{T_{f_{ull}}}{T_{max}} = \frac{\frac{S_f E_2^2 R_2}{R_2^2 + (S_f^2 X_2^2)}}{K \frac{E_2^2}{X_2^2} N - m}$ $\frac{T_{f_{ull}}}{T_{max}} = \frac{R_2 (2 \times X_2) S_f}{R_2^2 + S_f^2 \times X_2^2}$ Dividing both numerical & denoted by X ₂ ² : $\frac{T_{f_{ull}}}{T_{max}} = \frac{\frac{R_2 (2 \times X_2)}{X_2^2} \times S_f}{\frac{R_2^2}{X_2^2} + S_f^2 \times \frac{X_2^2}{X_2^2}}$ $\frac{T_{f_{ull}}}{T_{max}} = \frac{2 (R_2/X_2) S_f}{\frac{R_2^2}{X_2^2} + S_f^2}$ Let $a = R_2/X_2$ $\frac{T_{f_{ull}}}{T_{max}} = \frac{2 a \times S_f}{a^2 + S_f^2} - \cdots$	(1/2 Mark) (1/2 Mark) (1 Mark)
c)	Explain lamp method of synchronizing alternator to the bus ba	r.
2)	Following are the 'Three lamp method' of synchronizing an alternator	with the bus bar:-
	(Any One Lamp Method are expected: (Figure: 2 Mark	& Explanation: 2 Mark)
Ans:	1. All Dark lamp method or all bright lamp method:	
	Fig: For Three Phase Alternator	

MAHARASHTRA STATE BOARAD OF TECHNICAL EDUCATIOD (Autonomous) (ISO/IEC-27001-2005 Certified)

Winter– 2016 Examinations Model Answer

Page 30 of 40

Winter-2016 Examinations Model Answer Subject Code: 17511 Page 31 of 40 lamps are dark and the cross connected lamps are equally bright. OR Student may write this way BUS BAR INCOMING ALTERNATOR PARALLELING ▶ If the synchroscope is not available, synchronizing lamp method is used. > There are different methods of lamp connection. The method of two bright and one dark lamp indication is illustrated in above figure. > In this connection the lamps become bright and dark as follows for correct phase sequence. "Two lamps bright and one lamp dark at a time". > If all the lamps become simultaneously dark or bright, the phase sequence is wrong. > The switch is closed when the voltage, frequency and the lamps (2 bright and 1 Dark) satisfy the condition of synchronism. A total of 1200 kW is shared equally by two identical alternator at 6000 V and 0.866 **d**) lagging p.f., the current one alternator is 70 A at lagging p.f. find the p.f. of both the alternators. Both the alternators are 3 phase star connected. Total load: 1200 kW, Voltage: 6000V, P.f: 0.866 lag current of all = 70 A Solution: Step 1: Total active load (KW_L) = 1200 kW **Step 2 : Total reactive load :** $\therefore \phi = \cos^{-1}(0.866) = 30^{\circ}$ Elec. \therefore Total reactive load = 1200 kW × tan 30 Ans: :. Total reactiv load = 692.8203 KVAR ------ (1/2 Marks) **Step 3: Reactive Power shared by alternator 1:** $\therefore = P_1 \tan \phi_1 - \dots - (1/2 \text{ Marks})$ $\therefore P_1 = \sqrt{3} V_L \times I_L \times Cos\phi$

Subject Code: 17511	Winter– 2016 Examinations <u>Model Answer</u>	Page 32 of 40
	$\therefore \phi_1 = \cos^{-1}\left[\frac{1}{\sqrt{3} \times V_L \times I_L}\right]^{$	(1/2 Marks)
	$\therefore \phi_1 = Cos^{-1} [\frac{600 \times 10^3}{\sqrt{3} \times 6000 \times 70}]$	
	$\therefore \phi_1 = Cos - 1(34.431)$	
	$\therefore Cos \ \phi_1 = 0.8247 lag$	(1/2 Marks)
Reactive pow	ver shared by alternator $1 = 600 \times \tan (34.433)$	1)
	$= 411.3379 \ KVAR -$	(1/2 Marks)
Step 4: Reactive Po	wer shared by alternator 2 = Total reactive	– Reactive power of alt 1
	= 692.8203 - 41	1.3379
Reactive P	ower shared by alternator 2 = 281.4824 KV	/AR (1/2 Marks)
But,		
Reactive po	ower shared by alternator 2 = $P_1 \tan \phi_2$	
	$281.4824 = 600 \times \tan \phi$	9 ₂ (1/2 Marks)
	$\tan \phi_2 = \frac{281.4824}{600}$	
	$\tan \phi_2 = 0.4691$	
	$\phi_2 = \tan^{-1} (0.4691)$	
	$\phi_2 = 25.1331^{\circ}$	
	$\cos \phi_2 = 0.9053^0$	(1/2 Marks)
	OR student may write this way	
Step 1: Total active & 2	e load ($\mathbf{KW}_{\mathbf{L}}$) = 1200 kW is shared equally by	two indicate alternators 1

		Winter-2016 Ex	aminations
Subject C	ode: 17	7511 <u>Model An</u>	swer Page 34 of 40
	P	$\therefore \tan \phi_2 = \frac{l (FD)}{l (EF)} = 0.47 - \dots$ $\therefore \phi_2 = \tan^{-1} (0.47)$ $\therefore \phi_2 = 25.17$ $. \ Cos\phi_2 = P.f. \ of \ alternator \ 2$ ower factor alternator $\cos \phi_2 = 0.91$	
e) Dr	aw the	e torque-speed characteristics of l ons of linear induction motor and	inear induction motor. Write down any two universal motor.
Ans:	Appl	peed characteristics of linear indu	ction motor: (2 Marks)
S	r.No	Types of 1-Ph Induction Motor	Applications (Any Two expected)
		Linear Induction Motor (Any One Applications 1Marks)	 Application for Stationary Field System Automatic sliding doors in an electrical train, Metallic belt conveyer, Mechanical handling equipment, such as propulsion of a train of tubs along a certain route, Shuttle-propelling application.

	Winter– 2016 Ex	aminations
Subje	ct Code: 17511 <u>Model Ans</u>	wer Page 35 of 40
	2 Universal Motor (Any one Applications 1 Marks)	 Applications for the moving field system High and medium speed applications have been tried with linear motor propulsion of vehicles with air cushion or magnetic suspension. High speed application as a travelling crane motor where the field system is suspended from loist. 1) Mixer Food processor Heavy duty machine tools Grinder Vacuum cleaners Refrigerators Driving sewing machines Electric Shavers Hair dryers Small Fans Cloth washing machine portable tools like blowers, drilling machine, polishers etc
f)	What is induction generator? State its appli	actions
Ans:	Induction generator:	(2 Mark)
	When rotor of induction motor runs	faster than synchronous speed, induction
	motor runs as generator and called as induction	n generator. It converts mechanical energy it
	receives from the shaft into electrical energy w	hich is released by stator. However, for
	creating its own magnetic field, it absorbs reac	tive power Q from the lime to which it is
	connected. The reactive power is supplied by a	a capacitor bank connected at the induction
	generator output terminals.	
	Applications of Induction Generator:(And a second sec	ny Two Application expected: 1 Mark each)

ject Code	Winter- 2016 Examinations : 17511 <u>Model Answer</u> Page 37 of 40
	2. It must have an m.m.f. equal and opposite to that of armature reaction m.m.f.
	Any one Method are expected
1. Am	pere Turn Method (MMF Method) at Unity Power factor from graph:
\checkmark	Draw the line 'OA' to represent if which gives the rated generated voltage (V)
≻	'OC' represent field current required for producing full load current on short circuit OC =
	AB. Draw the line 'AB' at an angle (90) to represent if, which gives rated full load (Isc) on short circuit
\triangleright	Join the points 'O' and 'B' and find the field current (If) by measuring the distance 'OB'
	the gives the open circuit voltage (E ₀) from the open circuit characteristics.
\blacktriangleright	% Voltage Regulation = $\frac{E_0 - V}{V} \times 100$
2. Am	pere Turn Method (MMF Method) at Lagging Power factor from graph:
\triangleright	Draw the line 'OA' to represent if which gives the rated generated voltage (V)
\triangleright	'OC' represent field current required for producing full load current on short circuit
	OC = 'AB'. Draw the line 'AB' at an angle (90+ θ) to represent if, which gives rated
	full load (Isc) on short circuit
\triangleright	Join the points 'O' and 'B' and find the field current (If) by measuring the distance 'OB'
	the gives the open circuit voltage (E0) from the open circuit characteristics.
\blacktriangleright	% Voltage Regulation = $\frac{E_0 - V}{V} \times 100$
3. Am	pere Turn Method (MMF Method) at Leading Power factor from graph:
≻	Draw the line 'OA' to represent if which gives the rated generated voltage (V)
\succ	'OC' represent field current required for producing full load current on short circuit
	OC = 'AB'. Draw the line 'AB' at an angle (90- θ) to represent if, which gives rated
	full load (Isc) on short circuit
>	Join the points 'O' and 'B' and find the field current (If) by measuring the distance 'OB'
	the gives the open circuit voltage (E ₀) from the open circuit characteristics.
\succ	% Voltage Regulation = $\frac{E_0 - V}{V} \times 100$

Winter- 2016 Examinations Model Answer

Page 38 of 40

b)	Why single phase induction motor is not self starting ?
Ans:	Reason for single phase induction motors are not self starting:(4 Mark)
	 When single phase AC supply is given to main winding it produces alternating flux. According to double field revolving theory, alternating flux can be represented by two opposite rotating flux of half magnitude. These oppositely rotating flux induce current in rotor & there interaction produces two opposite torque hence the net torque is Zero and the rotor remains standstill. Hence Single-phase induction motor is not self starting. OR Single phase induction motor has distributed stator winding and a squirrel-cage rotor. When fed from a single-phase supply, its stator winding produces a flux (or field) which is only alternating i.e. one which alternates along one space axis only. It is not a synchronously revolving (or rotating) flux as in the case of a two or a three phase stator winding fed from a 2 of 3 phase supply. Now, alternating or pulsating flux acting on a stationary squirrel-cage rotor cannot produce rotation (only a revolving flux can produce rotation). That is why a single phase motor is not self-starting.
	Explain role of capacitor in a single phase capacitor start capacitor run induction
c)	motor. (Figure -2 Mark & Explanation -2 Mark)
Ans:	right 2 Hark C Explanation 2 Hark () for the formation of the format
	In these motors one capacitor is connected in series with the auxiliary winding. There is no

Winter-2016 Examinations **Model Answer** Subject Code: 17511 Page 40 of 40 State applications of the following : (any two) e) (i) DC servo motor (ii) Stepper motor. Ans: (i) Application of DC servo motor, It is widely used in : (Any Two Applications expected: 1 Mark each) 1. Radars 2. Computers 3. Robots 4. Machine Tools 5. Tracking and guidance systems 6. Process controllers (ii) Application of Stepper motor, It is widely used in : (Any Two Applications expected: 1 Mark each) 1. Suitable for use with computer control systems 2. Widely used in numerical control of machine tools 3. Tape Drives 4. Floppy disc Drives 5. Printers 6. X-Y Plotters 7. Robotics 8. Textile Industries 9. Integrated circuit fabrication 10. Electric Watches 11. In Space crafts launched for scientific explorations of planets. 12. In the production of science fiction movies. 13. Varity of commercial, medical and military applications

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