11718 4 Hours / 100 Marks

Saat	No	
Seat	INO.	

Instructions : (1) All questions are compulsory.

- (2) Answer each next main question on a new page.
- (3) Illustrate your answers with neat sketches wherever necessary.
- (4) Figures to the **right** indicate **full** marks.
- (5) Assume suitable values of $f_y, f_u, \gamma_{mo}, \gamma_{mw}$ if not given in question. (6) Use of Non-programmable Electronic Pocket Calculator is
- permissible.
- (7) Mobile Phone, Pager and any other Electronic Communication devices are not permissible in Examination Hall.

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1. A) Attempt **any three**.

a) State any four advantages of steel as a construction material.

b) Define:

- II) Zone factor
- IV) Fundamental natural period
- c) List the values of partial safety factor for material strength in case of resistance by yield, buckling, ultimate stress and bolt connection.
- d) Explain shear lag.

I) Importance factor

III) Response reduction factor

- B) Attempt any one.
 - a) Determine bolt value 16 mm diameter bolt of 4.6 grade to connect two angles $90 \times 60 \times 06$ mm back to back on opposite side of gusset plate of 8 mm thick. Also determine no. of bolts required for the joint when it carries direct factored load of 110 KN. Draw neat sketch of designed connection.
 - b) For a tension member as shown fig. 1. Determine block shear strength. $f_v = 250$ MPa, $f_{11} = 410$ MPa.



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2. Attempt any two.

a) Design suitable fillet welded connection for ISA $80 \times 50 \times 08$ mm with its longer leg connected to gusset plate of thickness 8 mm. The angle is subjected to factored load of 300 KN. $C_{xx} = 27.3$ mm. Assume weld applied to all three edges and shop weld.

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b) A built up column consist of 2ISMC – 225, placed face to face at 120 mm. The distance is between their centres. The length of column is 6.0 m and both end are hinged. Find design strength of column.

For single ISMC – 225

 $A = 3301 \text{ mm}^2$, $I_{YY} = 1.872 \times 10^6 \text{ mm}^4$,

 $I_{XX} = 26.946 \times 10^6 \text{ mm}^4$, $C_{XX} = 23.1 \text{ mm}$. (Refer table no. 1 for f_{cd})

c) An ISMB 400 @ 604.3 N/m is used as simply supported beam of span 5.0 M. The compression flange of the beam is laterally supported throughout the span. Determine design flexural strength of member. Also calculate working udl on the beam per meter span. Check the member for deflection.

Take $Z_p = 1176.18 \times 10^3 \text{ mm}^3$, $\gamma_{mo} = 1.1$, $\beta_b = 1.0$, $f_y = 250 \text{ MPa}$

3. Attempt any four.

- a) Explain any two types of failure of bolted joints with neat sketches.
- b) List types of bolts and sketch any one of them.
- c) Write the IS code provision for design of angle purlin.
- d) List the factors to be considered in calculation of wind load. Write equations to calculate wind load on roof truss as per IS 875-1987.
- e) Draw a neat labelled sketch of angle purlin with principle rafter at panel point having roof covering as A.C. sheets.

4. A) Attempt any three.

- a) State with sketch the effective length for a compression member as per IS 800/2007 having end conditions as
 - i) Translation restrained at both ends and rotation free at one end.
 - ii) Translation and rotation restrained at both ends.
- b) Draw neat sketch of lacing and battening. Also state function of same.
- c) Explain "Limits of width to thickness ratio to prevent buckling for a single angle strut. The limiting width to thickness ratio for a semi-compact class is 15.7 C. Check whether ISA $90 \times 90 \times 06$ mm is semi-compact class or not $f_v = 250$ MPa.
- d) What is local buckling in case of compression member ? What is its effect ? What is to be done to prevent it ?
- B) Attempt any one.
 - a) Explain gross section yielding and net section rupture in case of design strength of tension member. Also write two measures taken to prevent rupture.

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b) Design tension member consisting of single unequal angle connected to gusset plate of 12 mm thk. to carry a factored tensile load of 300 KN. Assume single row of 20 mm bolted connection. The length of the member is 2.5 m.

Take $f_u = 415 \text{ MPa} = 0.80$ Section (mm)Area (mm²)ISA $100 \times 75 \times 8$ 1336 $125 \times 75 \times 8$ 1588 $150 \times 75 \times 8$ 1748

5. Attempt any two.

- a) A hall of size 12 m × 20 m is provided with Howe type roof trusses at 4 m c/c. Calculate panel point load in case of DL and LL for following data
 - i) unit wt. of roof covering = 165 N/m^2
 - ii) self wt. of purlin = 100 N/m^2
 - iii) wt. of bracing = 60 N/m^2
 - iv) rise to span ratio = 1/5
 - v) total no. of panels = 08
- b) A industrial building has trusses for 14 m span. Trusses are spaced at 3.5 m c/c and rise of truss is 3.50 m. Calculate panel point load in case of live load and wind load using following data
 - i) Coefficient of external wind pressure $(C_{pe}) = -0.7$
 - ii) Coefficient of internal wind pressure $(C_{pi}^{r}) = \pm 0.2$
 - iii) Design wind pressure = 1200 N/m^2
 - iv) No. of panels = 08
- c) A column ISMB 300 carries an axial load of 1.5 MN. Design a slab base and concrete pedestal for the column. Take SBC of soil as 200 KPa and M20 grade of concrete is used for concrete pedestal. For ISMB 300 consider $b_f = 140 \text{ mm}$, $t_f = 13.1 \text{ mm}$. Take $f_v = 250 \text{ MPa}$,

 $\gamma_{mo} = 1.1.$

6. Attempt any four.

- a) Define laterally supported beam along with suitable sketch. State any three methods of providing lateral support to the beam.
- b) State four classification of c/s of beam based on moment-rotation behavior as per IS -800/2007.
- c) An ISMB 250 is used for simply supported span of 4 m to carry a factored load of 30 KN/m. Check the section for shear only. Take $f_v = 250$ MPa, $t_w = 6.4$ mm.
- d) Draw plan of gussetted base showing all components.
- e) Write steps to calculate the thickness of base plate used in slab base. Why anchor bolts are used in slab base.

KL/1 (SR)	• 40	50	60	70	80	90	100	110	120	130	140
fcd	198	183	168	152	136	121	107	94.6	83.7	74.3	66.2

Table – 1 : Values of design compressive stress (f_{cd}) for $f_v = 250$ MPa.

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IS:800-2007 Equations (Formula Sheet)

$$V_{nsb} = \left(\frac{f_u}{\sqrt{3}}\right) \left(n_n A_{nb} + n_s A_{sb}\right), \quad V_{dsb} = \frac{V_{nsb}}{\gamma_{mb}}, \quad V_{dpb} = \frac{V_{npb}}{\gamma_{mb}}$$

$$T_{dg} = \frac{A_g f_y}{\gamma_{m0}}, \quad T_{dn} = \frac{0.9 \text{ fu Art}}{\gamma_{m1}} \quad V_{npb} = 2.5 k_b dt f_u \quad k_b = \left[\frac{e}{3 \text{ do}}, \frac{p}{3 \text{ do}} - 0.25, \frac{f_{ub}}{f_u}, 1.0\right]$$

$$f_{wd} = \frac{f_u}{\sqrt{5} \text{ ymw}}$$

$$T_{dn} = \frac{0.9 A_{nc} f_u}{\gamma_{m1}} + \beta \frac{A_{go} f_y}{\gamma_{m0}} \quad \text{where} \quad \beta = 1.4 - 0.076 \text{ (w/t)} (f_y/f_u) (bs/L_c) \quad \leq (f_u \gamma_{mo}/f_y \gamma_{m1}) \times 0.9$$

$$\geq 0.7$$

$$T_{dn} = \frac{\alpha A_n f_u}{\gamma_{m1}} , \quad T_{db1} = \frac{A_{vg} f_y}{\sqrt{3} \gamma_{m0}} + \frac{0.9 A_{in} f_u}{\gamma_{m1}} , \quad T_{db2} = \frac{0.9 A_{vm} f_u}{\sqrt{3} \gamma_{m1}} + \frac{A_{ig} f_y}{\gamma_{m0}}$$

$$P_{d} = A_{e} f_{cd} , \qquad P_{z} = 0.6 V_{Z}^{2} , \qquad V_{z} = V_{b} k_{1} k_{2} k_{3}$$

$$f_{cd} = \chi \frac{f_{y}}{\gamma_{m0}} , \qquad \chi = \frac{1}{\phi + \sqrt{\phi^{2} - \lambda_{e}^{2}}} , \qquad \text{where } \phi = 0.5[1 + \alpha (\lambda_{e} - 0.2) + \lambda_{e}^{2}]$$

$$\lambda_{e} = \sqrt{k_{1} + k_{2} \lambda_{w}^{2} + k_{3} \lambda_{\phi}^{2}}$$

where $\lambda_{yv} = \frac{\left(\frac{l}{r_{w}}\right)}{s\sqrt{\frac{\pi^{2}E}{250}}} \text{ and } \lambda_{y} = \frac{(b_{1}+b_{2})/2t}{s\sqrt{\frac{\pi^{2}E}{250}}} \qquad Mz = \frac{\beta_{b} \cdot Z\rho \cdot fy}{\gamma^{2}mo}$ $Vdz = \frac{fy \times tw \times h}{\gamma^{2}mo \sqrt{3}}$

Values of χ and fcd (N/mm²) for different values of KL/r_{min} as per buckling curve 'c'

KL/r _{min}	10	20	30	40	50	60	70	80	90
X	1.000	0.987	0.930	0.870	0.807	0.740	0.670	0.600	0.533
fcd	227	224	211	198	183	168	152	136	121
	1	I	1	4	1	4	1		4
	L	I	1	l	I	L	I		L
KL/r _{min}	100	110	120	130	140	150	160	170	180
<u>KL/r_{min} X</u>	100 0.471	110 0.416	120 0.368	130	140 0.291	150 0.261	160 0.234	170 0.212	180 0.192