



Important Instructions to examiners:

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more importance. (Not applicable for subject English and Communication Skills.)
- 4) While assessing figures, examiner may give credit for principal components indicated in the figure. The figures drawn by the candidate and those in the model answer may vary. The examiner may give credit for any equivalent figure drawn.
- 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and the model answer.
- 6) In case of some questions credit may be given by judgment on part of examiner of relevant answer based on candidate's understanding.
- 7) For programming language papers, credit may be given to any other program based on equivalent concept.

Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.1	a)	Attempt any <u>SIX</u> of the following:		(12)
	i)	Define ductility and malleability.		
	Ans.	Ductility: It is the property of material due to which it can be drawn into thin wires on application of tensile force.	01	02
		Malleability: It is the property of a material by virtue of which it can be beaten up into thin sheets without cracking when hammered.	01	
	ii)	Define Principal plane and Principal stress.		
	Ans.	Principal plane: A plane which carries only normal stress and no shear stress is called Principal plane.	01	02
		Principal stress: The magnitude of normal stress acting on the principal plane is called Principal stress.	01	
iii)	Write the equation for M.I. of Hollow shaft section.			
Ans.	Hollow Shaft: $M.I. = \frac{\pi}{64} (D^4 - d^4)$ Where, D = External Daimeter d = Internal Daimeter	02	02	



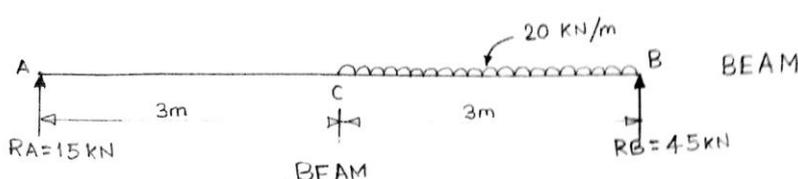
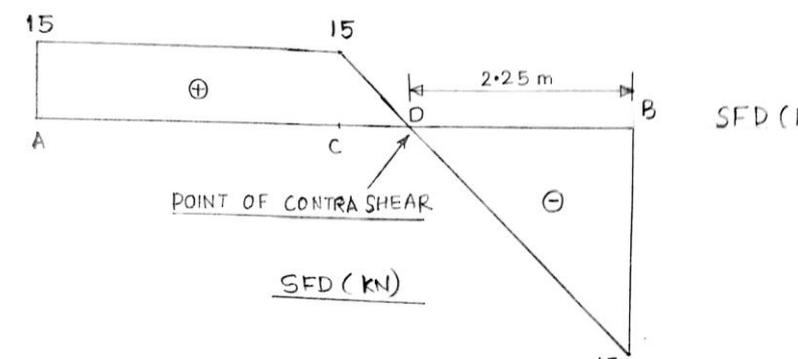
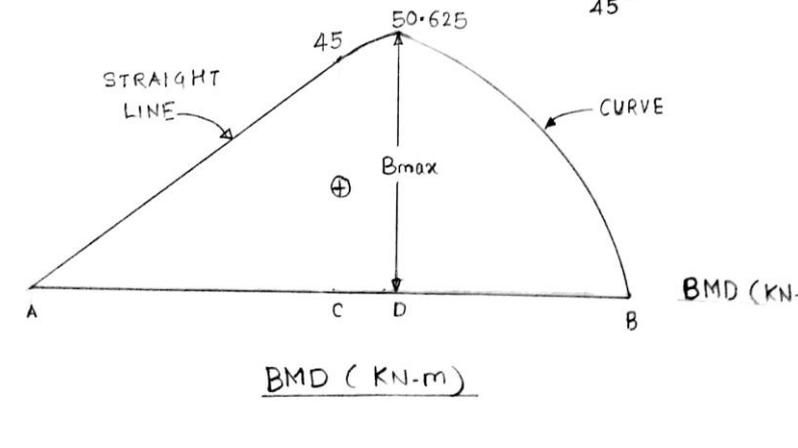
Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.1	iv)	Define direct load and eccentric load.		
	Ans.	Direct load: When a load whose line of action coincides with the axis of a member or whose line of action acts at a centroid of a section of member then it is called as a direct load.	01	02
		Eccentric load: A load acts away from the centroid of the section or a load whose line of action does not coincide with the axis of member is called as eccentric load.	01	
	v)	Write torsion equation along with meaning of each term used in it.		
	Ans.	$\frac{T}{I_p} = \frac{C.\theta}{L} = \frac{\sigma_s}{R} \quad \text{Or} \quad \frac{T}{J} = \frac{G.\theta}{L} = \frac{q_{\max}}{R}$ <p>Where,</p> <p>T = Twisting moment Or Torque Or Torsion (N-mm)</p> <p>$I_p = J$ = Polar Moment of Inertia (mm^4)</p> <p>C = G = Modulus of Rigidity for shaft material (N/mm^2)</p> <p>θ = Angle of twist (radians)</p> <p>L = Length of the shaft (mm)</p> <p>$\sigma_s = q_{\max}$ = Maximum shear stress (N/mm^2)</p> <p>R = Radius of the shaft (mm)</p>	01	02
			01	
vi)	Draw a stress- strain diagram for ductile material in tension.			
Ans.	<p>(i) Limit of proportionality (A) (ii) Elastic limit (B)</p> <p>(iii) Upper yield point (C) (iv) Lower yield point (D)</p> <p>(v) Ultimate (maximum) load point (E) (vi) Breaking point (F)</p>	01	02	
		01		



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.1	vii)	State relation between Hoop stress and Longitudinal stress, for thin cylinder.	02	02
	Ans.	$\sigma_c = 2\sigma_L$ Where, Hoop Stress (σ_c) = $\frac{Pd}{2t}$ Longitudinal stress (σ_L) = $\frac{Pd}{4t}$		
	viii)	Define core of section. Write its value for a circular section.		
	Ans.	Core of section: For no tension condition the load must lie within the middle third shaded area of eccentricity $2e$ is called core of section. The stress produced is only compressive stress. For circular section the core of section is $2e = \frac{D}{4}$ Where, e = Eccentricity of circular section D = Diameter of circular section		
		Attempt any TWO of the following:		(08)
	b)	For a round bar of 50 mm diameter and 2.5 m long of certain material has Young's modulus of $1.1 \times 10^5 \text{ N/mm}^2$ and Modulus of rigidity of $0.45 \times 10^5 \text{ N/mm}^2$. Find the Bulk modulus and the lateral contraction of the bar when stretched by 3 mm.		
	(i)			
	Ans.	Given: d = 50mm, L = 2.5m E = $1.1 \times 10^5 \text{ N/mm}^2$, G = $0.45 \times 10^5 \text{ N/mm}^2$, $\delta L = 3 \text{ mm}$ Find : K, δd $E = 2G(1 + \mu)$ $1.1 \times 10^5 = 2 \times 0.45 \times 10^5 (1 + \mu)$ $\mu = 0.22$ $E = 3K(1 - 2\mu)$ $1.1 \times 10^5 = 3 \times K(1 - 2 \times 0.22)$ $K = 65476.190 \text{ N/mm}^2$ $K = 0.65 \times 10^5 \text{ N/mm}^2$	01	
			01	



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.1	b)	$\mu = \frac{\text{Lateral Strain}}{\text{linear Strain}}$ $\text{Lateral Strain} = \mu \times \text{linear Strain}$ $\left(\frac{\delta d}{d}\right) = \mu \times \left(\frac{\delta L}{L}\right)$ $\left(\frac{\delta d}{50}\right) = 0.22 \times \left(\frac{3}{2500}\right)$ $\boxed{\delta d = 0.0132mm}$	01	04
	ii)	<p>A simply supported beam 6 m long is carrying a udl of 20 kN/m over a length of 3 m from the right end. Draw the SFD and BMD for the beam and also calculated the maximum bending moment in the section.</p>		
	Ans.	<p>Step I Calculation of reactions</p> $\sum M_A = 0$ $R_B \times 6 = 20 \times 3 \times (3+1.5)$ $\boxed{R_B = 45 \text{ kN}}$ $\sum F_y = 0$ $R_A + R_B = 20 \times 3$ $R_A + 45 = 60$ $\boxed{R_A = 15 \text{ kN}}$ <p>Step II SF Calculations</p> <p>SF at A = +15 kN</p> $C_L = +15 \text{ kN}$ $B_L = +15 - 60 = -45 \text{ kN}$ $B_R = -45 + 45 = 0 \quad (\therefore \text{ok})$	1/2	
			1/2	

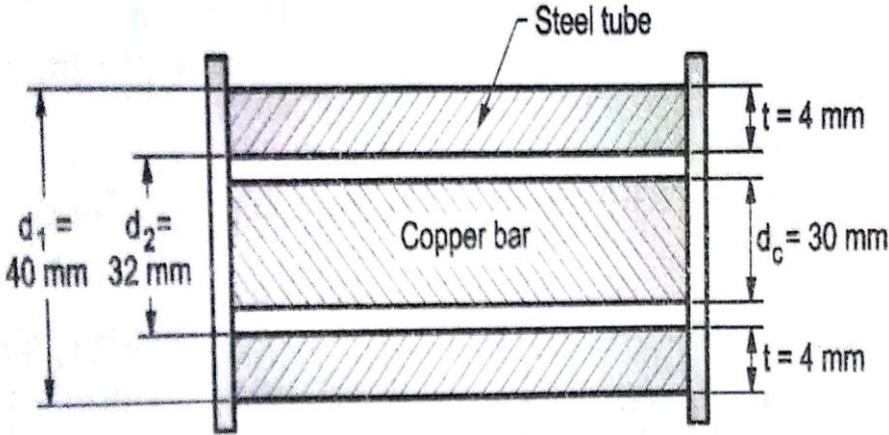
Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.1	b)	<p>Step III</p> <p>BM Calculations</p> <p>BM at A and B = 0 (Supports are simple)</p> <p>BM at C = + 15×3 = + 45 kN-m</p> <p>To calculate B_{max}</p> <p>SF is Zero at B_{max} ∴ 20x + 45 = 0</p> <p>∴ x = 2.25m from support B</p> $B_{\max} = + 45 \times 2.25 - 20 \times \frac{(2.25)^2}{2} = +50.625 \text{ kN-m}$ <div style="border: 1px solid black; padding: 2px; display: inline-block;"> $B_{\max} = 50.625 \text{ kN-m}$ </div>   	01	04
			01	
			01	



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.1	iii)	<p>A cantilever beam of span 6.5 m is having cross section of 400 mm wide and 700 mm deep. If the bending stress is not allowed to exceed 280 N/mm², calculate the magnitude of point load which can be applied at the free end of the cantilever beam.</p> <p>Ans.</p> <p>Given:</p> <p>$L = 6.5\text{m}, \quad b = 400\text{mm},$ $d = 700\text{mm}, \quad \sigma_b = 280\text{N/mm}^2$</p> <p>Find: 'W' at free end</p> <p>$M = (W \times L) \text{N-m}$</p> <p>$M = (6.5 \times 10^3) W \text{ N-mm}$</p> <p>$I = \frac{bd^3}{12} = \frac{400 \times 700^3}{12}$</p> <p>$I = 1.143 \times 10^{10} \text{ mm}^4$</p> <p>$y = \frac{d}{2} = \frac{700}{2} = 350\text{mm}$</p> <p>$\sigma_b = \left(\frac{M}{I}\right) \times y$</p> <p>$280 = \left(\frac{(6.5 \times 10^3) W}{1.143 \times 10^{10}}\right) \times 350$</p> <p>$W = 1407179.487 \text{ N}$</p> <p>$W = 1407.179 \text{ kN}$</p>	<p>1/2</p> <p>01</p> <p>1/2</p> <p>01</p> <p>01</p>	04
Q.2	a)	<p>Attempt any <u>FOUR</u> of the following:</p> <p>a) A metal rod, 500 mm long and 20 mm in diameter is subjected to an axial pull of 40 kN. Under this load, elongation of rod is 0.5 mm and decrease in diameter of rod is 0.006 mm. Calculate modulus of elasticity and Poisson's ratio.</p> <p>Ans.</p> <p>Given:</p> <p>$P = 40\text{kN}, \quad L = 500\text{mm},$ $d = 20\text{mm}, \quad \delta L = 0.5\text{mm},$ $\delta d = 0.006 \text{ mm}$</p> <p>Find: E, μ</p> <p>$A = \frac{\pi}{4} d^2 = \frac{\pi}{4} (20)^2 = 314.16\text{mm}^2$</p> <p>$E = \frac{PL}{A\delta L}$</p>	01	(16)



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.2		$E = \frac{40 \times 10^3 \times 500}{314.16 \times 0.5} = 127323.9545 \text{ N/mm}^2$ $E = 1.2732 \times 10^5 \text{ N/mm}^2$ $\mu = \frac{\text{Lateral Strain}}{\text{linear Strain}}$ $\mu = \frac{\left(\frac{\delta d}{d}\right)}{\left(\frac{\delta L}{L}\right)} = \frac{\left(\frac{0.006}{20}\right)}{\left(\frac{0.5}{500}\right)}$ $\mu = 0.3$	01 01 01	04
	b)	<p>A hollow steel tube 200 mm external diameter and 25 mm thick is 4 m long used as a column. If it's one end is fixed and other end is hinged, find the load the column can carry. Use Euler's formula and FOS = 2, Take E = 2x10⁵ N/mm².</p>		
	Ans.	<p>Given:</p> <p>D = 200mm, t = 25mm, L = 4 m, E = 2x10⁵ N/mm², FOS = 2</p> <p>Find: P_{safe}</p> <p>d = (D - 2t) = (200 - 2x25) = 150mm</p> <p>Le = $\frac{L}{\sqrt{2}} = \frac{4000}{\sqrt{2}} = 2828.427\text{mm}$</p> <p>I_{min} = $\frac{\pi}{64} (D^4 - d^4) = \frac{\pi}{64} (200^4 - 150^4)$</p> $I_{\min} = 53689327.58 \text{ mm}^4$ <p>P = $\frac{\pi^2 EI_{\min}}{(Le)^2}$</p> <p>P = $\frac{\pi^2 \times 2 \times 10^5 \times 53689327.58}{(2828.427)^2}$</p> <p>P = 13247310.59 N</p> <p>P_{Safe} = $\frac{P}{\text{FOS}} = \frac{13247310.59}{2}$</p> <p>P_{Safe} = 6623655.3 N</p> $P_{\text{Safe}} = 6.624 \times 10^3 \text{ kN}$	1/2 1/2 01 01 01	04

Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.2	c)	<p>A steel tube 40 mm external diameter and 4 mm thick encloses centrally a solid copper bar of 30 mm diameter. The bar and the tube are rigidly connected together at the ends at a temperature of 40°C. Find the stress and its nature in each metal when heated to 180 °C. Take $\alpha_s = 1.08 \times 10^{-5}/^\circ\text{C}$, $\alpha_c = 1.7 \times 10^{-5}/^\circ\text{C}$, $E_s = 2.1 \times 10^5 \text{ N/mm}^2$ and $E_c = 1.1 \times 10^5 \text{ N/mm}^2$.</p>		
	Ans.	 <p><i>Given :</i></p> $T_1 = 40^\circ\text{C}, \quad T_2 = 180^\circ\text{C},$ $\alpha_s = 1.08 \times 10^{-5}/^\circ\text{C}, \quad \alpha_c = 1.7 \times 10^{-5}/^\circ\text{C},$ $E_s = 2.1 \times 10^5 \text{ N/mm}^2, \quad E_c = 1.1 \times 10^5 \text{ N/mm}^2$ <p><i>Find :</i> σ_s, σ_c</p> $t = T_2 - T_1$ $t = 180 - 40$ $\boxed{t = 140^\circ\text{C}}$ $A_s = \frac{\pi}{4}(D^2 - d^2)$ $A_s = \frac{\pi}{4}(40^2 - 32^2)$ $\boxed{A_s = 452.39 \text{ mm}^2}$ $A_c = \frac{\pi}{4}(d)^2$ $A_c = \frac{\pi}{4}(30)^2$ $\boxed{A_c = 706.86 \text{ mm}^2}$	1/2	
			1/2	
			1/2	

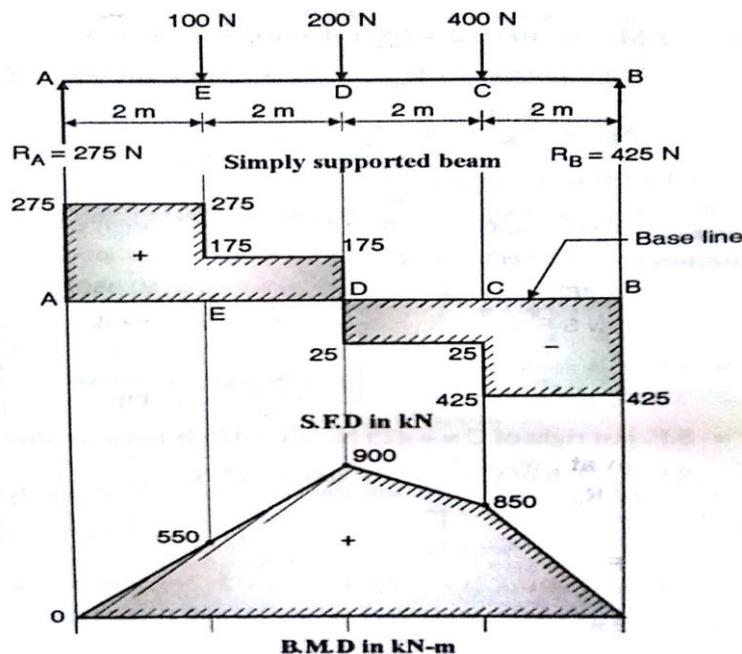


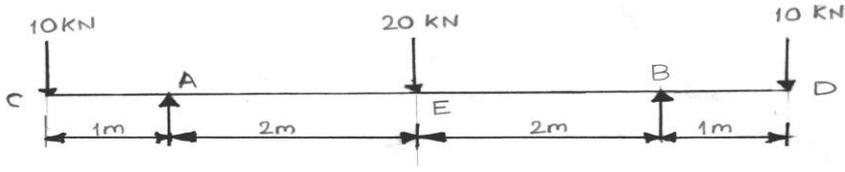
Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.2		$P_s = P_c$ $\sigma_s A_s = \sigma_c A_c$ $\sigma_s = \left(\frac{A_c}{A_s} \right) \sigma_c$ $\sigma_s = \left(\frac{706.86}{452.39} \right) \sigma_c$ $\sigma_s = 1.5625 \sigma_c$ $\frac{\sigma_s}{E_s} + \frac{\sigma_c}{E_c} = (\alpha_c - \alpha_s) t$ $\frac{1.5625 \sigma_c}{2.1 \times 10^5} + \frac{\sigma_c}{1.1 \times 10^5} = (1.7 \times 10^{-5} - 1.08 \times 10^{-5}) \times 140$ $\sigma_c = 52.51 \text{ N/mm}^2 \text{ (C)}$ $\sigma_s = (1.5625) \sigma_c$ $\sigma_s = 1.5625 \times 52.51$ $\sigma_s = 82.046 \text{ N/mm}^2 \text{ (T)}$	<p>1/2</p> <p>1/2</p> <p>1/2</p> <p>1/2</p>	04
	<p>d) A steel tube of 40 mm inside diameter and 4 mm metal thickness is filled with concrete. Determine the stress in each material due to an axial thrust of 60 kN. Take $E_{\text{steel}} = 2.1 \times 10^5 \text{ N/mm}^2$ and $E_{\text{con}} = 0.14 \times 10^5 \text{ N/mm}^2$</p> <p>Ans. Given:</p> <p>$P = 60 \text{ kN}$, $d = 40 \text{ mm}$</p> <p>$t = 4 \text{ mm}$, $E_s = 2.1 \times 10^5 \text{ N/mm}^2$</p> <p>$E_c = 0.14 \times 10^5 \text{ N/mm}^2$</p> <p>Find: σ_c, σ_s</p> <p>External diameter,</p> <p>$D = d + 2t$</p> <p>$D = 40 + (2 \times 4)$</p> $D = 48 \text{ mm}$ $A_s = \frac{\pi}{4} (D^2 - d^2)$ $A_s = \frac{\pi}{4} (48^2 - 40^2)$ $A_s = 552.92 \text{ mm}^2$	<p>1/2</p> <p>1/2</p>		

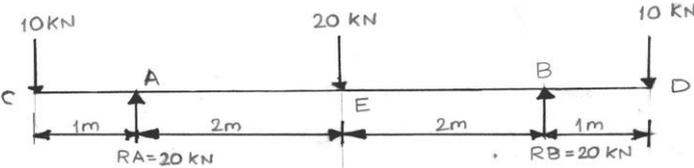
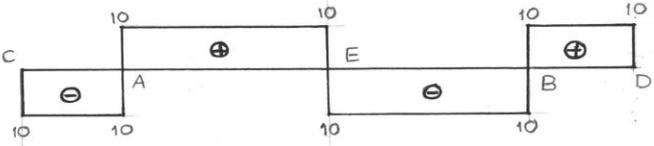
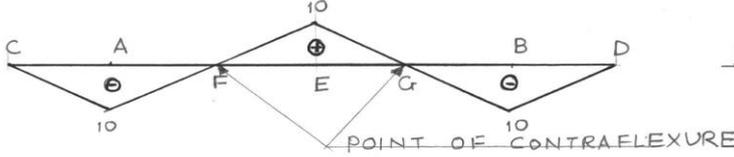
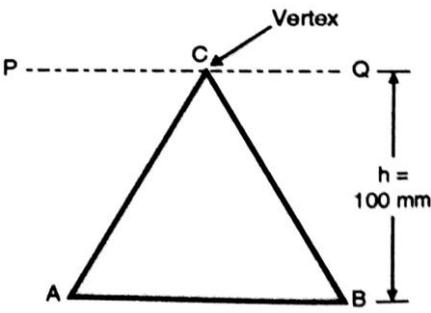


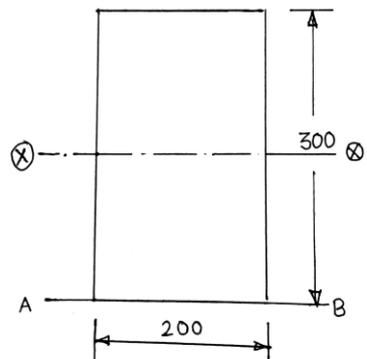
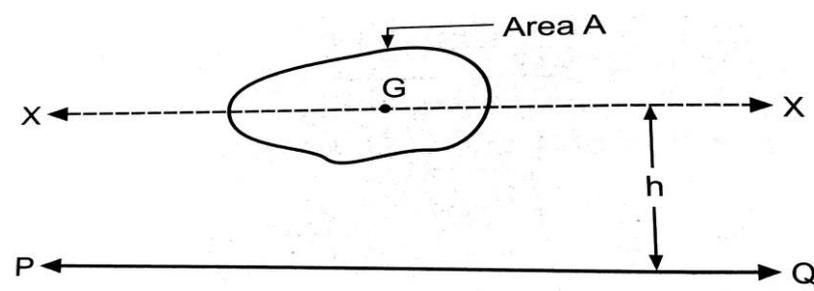
Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.2		$A_c = \frac{\pi}{4} d^2$ $A_c = \frac{\pi}{4} (40)^2$ $A_c = 1256.637 \text{mm}^2$	1/2	04
		$\frac{\sigma_s}{E_s} = \frac{\sigma_c}{E_c}$ $\sigma_s = \left(\frac{E_s}{E_c} \right) \times \sigma_c$ $\sigma_s = \left(\frac{2.1 \times 10^5}{0.14 \times 10^5} \right) \times \sigma_c$ $\sigma_s = 15 \sigma_c$	1/2	
		$P = P_s + P_c$ $P = \sigma_s A_s + \sigma_c A_c$ $60 \times 10^3 = (15 \sigma_c) \times 552.92 + \sigma_c \times 1256.637$ $\sigma_c = 6.28 \text{N/mm}^2$	1/2	
		$\sigma_s = 15 \sigma_c$ $\sigma_s = 15 \times 6.28$ $\sigma_s = 94.236 \text{N/mm}^2$	1/2	
	e)	<p>A bar is subjected to a tensile stress of 100 N/mm². Determine the normal and tangential stresses on a plane making an angle of 60° with the axis of tensile stress.</p>		
	Ans.	<p>Given:</p> $\sigma_x = 100 \text{N/mm}^2 \quad \theta = 90^\circ - 60^\circ = 30^\circ$ <p>Find: σ_n, σ_t</p> $\sigma_n = \sigma_x \cos^2 \theta$ $\sigma_n = 100 \times \cos^2 30$ $\sigma_n = 75 \text{N/mm}^2 (T)$	01	
		$\sigma_t = \frac{\sigma_x}{2} \sin 2\theta$ $\sigma_t = \frac{100}{2} \times \sin (2 \times 30)$ $\sigma_t = 43.30 \text{N/mm}^2$	01	
			01	
			01	
			01	

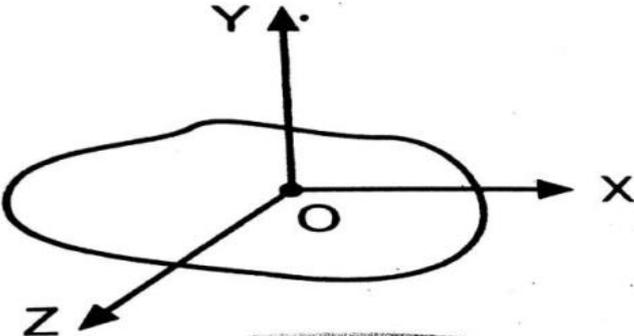
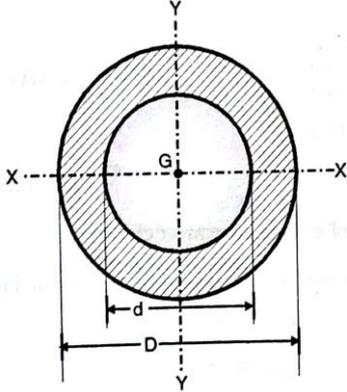
Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.3		$\Sigma F_y = 0$ $R_A + R_B - 100 - 200 - 400 = 0$ $R_A + 425 - 100 - 200 - 400 = 0$ $R_A = 275 \text{ N } \uparrow$ Step II S. F. Calculations SF at A = + 275 N $E_L = + 275 \text{ N}$ $E_R = + 275 - 100 = + 175 \text{ N}$ $D_L = + 175 \text{ N}$ $D_R = + 175 - 200 = - 25 \text{ N}$ $C_L = - 25 \text{ N}$ $C_R = - 25 - 400 = - 425 \text{ N}$ $B_L = - 425 \text{ N}$ $B = - 425 + 425 = 0 \quad (\because \text{ok})$ Step III B. M. Calculations BM at A and B = 0 $(\because \text{Supports are simple})$ BM at E = $275 \times 2 = + 550 \text{ kN-m}$ BM at D = $+ 275 \times 4 - 100 \times 2 = + 900 \text{ kN-m}$ BM at C = $+ 425 \times 2 = + 850 \text{ kN-m}$	01	
			01	
			01	04



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.3	e)	<p>A simply supported beam having equal overhangs on both sides and carrying point loads is shown in Fig. No. 1. Draw SF and BM diagrams.</p>  <p style="text-align: center;">Fig. No. 1</p>		
	Ans.	<p>Step I</p> <p>Calculate support reactions, Due to symmetrical loading, $R_A = R_B$</p> $R_A = R_B = \left(\frac{10 + 20 + 10}{2} \right) = 20 \text{ kN}$ <p style="text-align: center;">Or</p> $\Sigma M_A = 0$ $(R_B \times 4) + (10 \times 1) = (20 \times 2) + (10 \times 5)$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">$R_B = 20 \text{ kN}$</div> $\Sigma F_Y = 0$ $R_A + R_B = 40$ $R_A + 20 = 40$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">$R_A = 20 \text{ kN}$</div> <p>Step II</p> <p>S. F. Calculations</p> <p>SF at $C_R = -10 \text{ kN}$</p> $A_L = -10 \text{ kN}$ $A_R = +10 + 20 = +10 \text{ kN}$ $E_L = +10 \text{ kN}$ $E_R = +10 - 20 = -10 \text{ kN}$ $B_L = -10 \text{ kN}$ $B_R = -10 + 20 = +10 \text{ kN}$ $D_L = +10 \text{ kN}$ $D_R = -10 - 10 = 0 \quad (\therefore \text{ok})$	01	

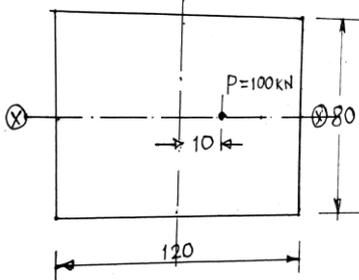
Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.3		<p>Step III</p> <p>B. M. Calculations</p> <p>BM at C and D = 0 (\because free end)</p> <p>BM at A = $-10 \times 1 = -10$ kN-m</p> <p>BM at E = $-10 \times 3 + 20 \times 2 = +10$ kN-m</p> <p>BM at B = $-10 \times 1 = -10$ kN-m</p>  <p>BEAM</p>  <p>SFD (KN)</p>  <p>BMD (kN-m)</p> <p>POINT OF CONTRAELEXURE</p>	01	04
f)		<p>Calculate M.I. for a triangle of height 100 mm about axis passing through vertex and parallel to base. If M.I. about the base of same triangle is 10^7 mm⁴.</p>	01	
Ans.		<p>Given:</p> <p>$I_{\text{base}} = 10^7$ mm⁴,</p> <p>Height of Triangle (h) = 100 mm</p> <p>Find: I_{vertex}</p> <p>Step I</p> <p>Calculate base width (b) of Triangle</p> $I_{\text{base}} = \frac{bh^3}{12}$ $10^7 = \frac{b \times 100^3}{12}$ $b = \frac{10^7 \times 12}{100^3} = 120 \text{ mm}$ <p>$b = 120 \text{ mm}$</p> <p>Step II : Calculate I_{vertex}</p> $I_{\text{vertex}} = \frac{bh^3}{4} = \frac{120 \times 100^3}{4} = 3 \times 10^7 \text{ mm}^4$ <p>$I_{\text{vertex}} = 3 \times 10^7 \text{ mm}^4$</p> 	01	04
			01	
			01	
			01	

Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.4		<p>Attempt any FOUR of the following:</p> <p>a) A rectangular beam section has width 200 mm depth of 300 mm. Using parallel axis theorem. Calculate M.I. about its base.</p> <p>Ans. M.I. of rectangle about its base (I_{AB}) Using parallel axis theorem, $I_{AB} = I_G + Ah^2$ $= I_{XX} + Ah^2$ $= \frac{bd^3}{12} + bd \times \left(\frac{d}{2}\right)^2$ $= \frac{200 \times 300^3}{12} + (200 \times 300 \times (150)^2)$ <div style="border: 1px solid black; padding: 2px; display: inline-block;">$I_{AB} = 1.8 \times 10^9 \text{ mm}^4$</div></p> 	02	(16)
		<p>b) State parallel axis theorem and perpendicular axis theorem of moment of inertia with neat sketches.</p> <p>Ans. a) Parallel axis theorem: It states that the M. I. of a plane section about any axis parallel to the centroidal axis is equal to the M. I. of the section about the centroidal axis plus the product of the area of the section and square of the distance between the two axes.</p>  <div style="border: 1px solid black; padding: 2px; display: inline-block;">$I_{PQ} = I_G + Ah^2$</div>	02	
		<p>b) Perpendicular axis theorem: It state, if I_{XX} and I_{YY} are the moments inertia of a plane section about the two mutually perpendicular axes meeting at O, then the moment of inertia about the third axis Z-Z i.e. I_{ZZ} is equal to addition of moment of inertia about X-X and Y-Y axes.</p>	01	04

Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.4		 $I_P = I_{ZZ} = I_{XX} + I_{YY}$	01	
	c)	<p>A hollow C.I. pipe, with external diameter 100 mm and thickness of metal 10 mm is used as a strut. Calculate the moment of inertia and radius of gyration about its diameter.</p>		
	Ans.	<p>Given:</p> <p>$D = 100 \text{ mm}, t = 10 \text{ mm},$</p> <p>1) $D = 100 \text{ mm},$ $d = D - 2t = 100 - (2 \times 10) = 80 \text{ mm}$</p> <p>2) Area of strut $A = \frac{\pi}{4}(D^2 - d^2)$ $= \frac{\pi}{4}(100^2 - 80^2)$ $A = 2827.43 \text{ mm}^2$</p> <p>3) M.I. about diameter (I_{XX} or I_{YY}) $I_{XX} \text{ or } I_{YY} = \frac{\pi}{64}(D^4 - d^4)$ $= \frac{\pi}{64}(100^4 - 80^4)$ $I_{XX} \text{ or } I_{YY} = 2898119.223 \text{ mm}^4$</p> <p>4) Radius of gyration, $K_{XX} \text{ or } K_{YY} = \sqrt{\frac{I_{XX}}{A}} = \sqrt{\frac{2898119.223}{2827.43}}$ $K_{XX} \text{ or } K_{YY} = 32.015 \text{ mm}$ $K_{XX} \text{ or } K_{YY} = 32.015 \text{ mm}$</p>	<p>1/2</p> <p>1/2</p> <p>01</p> <p>1/2</p> <p>01</p>	
				

Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.4	d)	<p>Find the M.I. of an I-section having equal flanges 120 mm x 40 mm and web 120 mm x 40 mm about XX- axis overall depth 200 mm.</p>	02	04
	Ans.	<p>M.I. at x-x axis,</p> $I_{xx} = \frac{BD^3}{12} - \frac{bd^3}{12}$ $= \frac{120 \times 200^3}{12} - \frac{80 \times 120^3}{12}$ <div style="border: 1px solid black; padding: 2px; display: inline-block;"> $I_{xx} = 68.48 \times 10^6 \text{ mm}^4$ </div> <p style="text-align: center;">OR</p> <p>Due to symmetry of section ,</p> $\bar{x} = \frac{120}{2} = 60 \text{ mm},$ $\bar{y} = \frac{200}{2} = 100 \text{ mm},$ <p>M.I. at x-x axis</p> $I_{xx} = I_{xx_1} + I_{xx_2} + I_{xx_3}$ $I_{xx} = (I_{G_1} + A_1 h_1^2) + (I_{G_2} + A_2 h_2^2) + (I_{G_3} + A_3 h_3^2)$ $I_{G_1} = \frac{b_1 d_1^3}{12} = \frac{120 \times 40^3}{12} = 640000 \text{ mm}^4$ $I_{G_2} = \frac{b_2 d_2^3}{12} = \frac{40 \times 120^3}{12} = 5760000 \text{ mm}^4$ $I_{G_3} = \frac{b_3 d_3^3}{12} = \frac{120 \times 40^3}{12} = 640000 \text{ mm}^4$ $A_1 = 120 \times 40 = 4800 \text{ mm}^2$ $A_2 = 40 \times 120 = 4800 \text{ mm}^2$ $A_3 = 120 \times 40 = 4800 \text{ mm}^2$ $h_1 = \bar{y} - y_1 = 100 - 20 = 80 \text{ mm}$ $h_2 = \bar{y} - y_2 = 100 - 100 = 0$ $h_3 = y_3 - \bar{y} = 180 - 100 = 80 \text{ mm}$ $I_{xx} = (I_{G_1} + A_1 h_1^2) + (I_{G_2} + A_2 h_2^2) + (I_{G_3} + A_3 h_3^2)$ $I_{xx} = (640000 + 4800 \times 80^2) + (5760000 + 4800 \times 0^2) + (640000 + 4800 \times 80^2)$ <div style="border: 1px solid black; padding: 2px; display: inline-block;"> $I_{xx} = 68.48 \times 10^6 \text{ mm}^4$ </div>		
			02	04
			01	OR
			01	04
			01	04

Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.4	e)	<p>Explain the meaning of moment of resistance and neutral axis in the theory of simple bending.</p> <p>Ans.</p> <p>Moment of resistance: Moment of resistance of the beam is the moment of couple formed by the total compressive force acting at the Centre of gravity of the compressive stress diagram and the total tensile force acting at the Centre of gravity of the tensile stress diagram. Moment of couple = $C \times Z$ or $T \times Z$. This moment is called the moment of resistance of the beam and is denoted by M_r.</p> <p>Neutral Axis: The fibers in the lower part of the beam undergo elongation while those in the upper part are shortened. These changes in the lengths of the fibers set up tensile and compressive stresses in the fibers. The fibers in the centroidal layer are neither shortened nor elongated. These centroidal layers which do not undergo any extension or compression is called neutral layer or neutral surface. When the beam is subjected to pure bending there will always be one layer which will not be subjected to either compression or tension. This layer is called as neutral layer and axis of this layer is called Neutral Axis.</p>	01 01 01	04

Que. No.	Sub. Que.	Model Answers	Marks	Total Marks	
Q.4	f)	<p>The cross section of beam is symmetrical I- section having flange width 100 mm, overall depth 180 mm and thickness 10 mm. If the permissible bending stress is 120 N/mm², find the moment of resistance of the beam section.</p> <p>Ans.</p> <p>Given: $\sigma_b = 120 \text{ N/mm}^2$ Find : M_r</p> $I = \left[\frac{BD^3}{12} - \frac{bd^3}{12} \right]$ $I = \left[\frac{100 \times 180^3}{12} - \frac{90 \times 160^3}{12} \right]$ $I = 17.88 \times 10^6 \text{ mm}^4$ $y = \frac{180}{2} = 90 \text{ mm}$ <p>Using flexural formula, $\frac{M}{I} = \frac{\sigma_b}{y}$</p> <p>Moment of resistance, $M_r = \left(\frac{\sigma_b}{y} \right) \times I$ $= \left(\frac{120}{90} \right) \times 17.88 \times 10^6$</p> $M_r = 23.84 \times 10^6 \text{ N - mm}$	<p>1/2</p> <p>01</p> <p>1/2</p> <p>01</p> <p>01</p>	04	
Q.5	a)	<p>Attempt any <u>FOUR</u> of the following:</p> <p>a) A rectangular strut is 120 mm x 80 mm thick. It carries a load of 100 kN at an eccentricity of 10 mm in a plane bisecting the thickness. Find the maximum and minimum intensities of stress in the strut section.</p> <p>Ans.</p> <p>Given: $b = 120 \text{ mm}$, $d = 80 \text{ mm}$, $e = 10 \text{ mm}$ $P = 100 \text{ kN} = 100 \times 10^3 \text{ N}$ Find: σ_{\max}, σ_{\min}</p> <p>Direct Stress, $\sigma_o = \frac{P}{A}$ $\sigma_o = \frac{100 \times 10^3}{120 \times 80}$</p> $\sigma_o = 10.417 \text{ N/mm}^2$		01	(16)



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.5	c)	$\sigma_o = \frac{P}{A}$ $\sigma_o = \frac{4 \times 10^3}{60 \times 20}$ $\sigma_o = 3.334 \text{ N/mm}^2$	01	04
		<p>Bending stress,</p> $\sigma_b = \frac{M}{I} \times Y$ $\sigma_b = \frac{P \cdot e}{db^3} \times \frac{b}{2}$ $\sigma_b = \frac{4 \times 10^3 \times 200}{20 \times 60^3} \times \frac{60}{2}$ $\sigma_b = 66.667 \text{ N/mm}^2$	01	
		<p>Maximum stress,</p> $\sigma_{\max} = \sigma_o + \sigma_b$ $\sigma_{\max} = 3.334 + 66.667$ $\sigma_{\max} = 70.001 \text{ N/mm}^2 \text{ (T)}$	1/2	
		<p>Minimum stress,</p> $\sigma_{\min} = \sigma_o - \sigma_b$ $\sigma_{\min} = 3.334 - 66.667$ $\sigma_{\min} = -63.333 \text{ N/mm}^2$ $\sigma_{\min} = 63.333 \text{ N/mm}^2 \text{ (C)}$	1/2	
	d)	<p>A M.S. link as shown in Fig. No. 3 transmits a pull of 80 kN. Find the cross sectional dimensions (band t) if $b = 3t$. Assume the permissible tensile stress as 70 MPa.</p>		
	Ans.	<p>Given:</p> $P = 80 \text{ kN} = 80 \times 10^3 \text{ N}$ $\sigma = 70 \text{ MPa} = 70 \text{ N/mm}^2$ $e = \frac{b}{2}, \quad b = 3t$ <p>Find: b, t</p> $\sigma = \sigma_o + \sigma_b$ $\sigma = \frac{P}{A} + \frac{P \cdot e}{I} \times Y$		



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.5		$\sigma = \frac{P}{A} + \frac{P.e}{\left(\frac{t \times b^3}{12}\right)} \times \frac{b}{2}$ $70 = \frac{80 \times 10^3}{b \times t} + \frac{80 \times 10^3 \times \frac{b}{2} \times b \times 6}{t \times b^3}$ <p>Put $b = 3t$</p> $70 = \frac{80 \times 10^3}{3t \times t} + \frac{80 \times 10^3 \times \frac{3t}{2} \times 3t \times 6}{t \times 3t}$ $t^2 = \frac{320 \times 10^3}{70 \times 3}$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">t = 39.036 mm</div> $b = 3 \times 39.036$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">b = 117.108 mm</div>	01	04
	e)	<p>A circular section of diameter 'd' is subjected to load 'P' eccentric to the axis-YY. The eccentricity of loads is 'e'. Obtain the limit of eccentricity such that no tension is induced at the section.</p>	01	
	Ans.	$A = \frac{\pi}{4} d^2, I = \frac{\pi}{64} d^4, Y = \frac{d}{2}$ <p>For no tension condition,</p> $\sigma_0 = \sigma_b$ $\frac{P}{A} = \frac{M}{Z}$ $\frac{P}{A} = \frac{P \times e}{\left(\frac{I}{Y}\right)}$	01	
		$e = \left(\frac{1}{A}\right) \times \left(\frac{I}{Y}\right) = \left(\frac{1}{\frac{\pi}{4} d^2}\right) \times \left(\frac{\frac{\pi}{64} d^4}{\frac{d}{2}}\right)$ $e = \frac{d}{8}$ $2e = \frac{d}{4}$	01	
		<p>Limit of eccentricity $2e = \frac{d}{4}$</p>	01	



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.5	f)	<p>A short MS column of external diameter 200 mm and internal diameter 150 mm carries an eccentric load. Find the greatest eccentricity which the load can have without producing tension in the section of a column.</p> <p>Ans. Given: External Diameter, D = 200 mm Internal Diameter, d = 150 mm Find: P, e For no tension condition, $\sigma_0 = \sigma_b$ $\frac{P}{A} = \frac{M}{Z}$ $\frac{P}{A} = \frac{P.e.Y}{I}$ $e = \frac{I}{A.Y}$ $e = \frac{\left(\frac{\pi}{64} \times (D^4 - d^4)\right)}{\left(\frac{\pi}{4} \times (D^2 - d^2) \times \frac{D}{2}\right)} = \frac{\left(\frac{\pi}{64} \times (200^4 - 150^4)\right)}{\left(\frac{\pi}{4} \times (200^2 - 150^2) \times \frac{200}{2}\right)}$ e = 39.0625 mm <div style="border: 1px solid black; padding: 2px; display: inline-block;">Greatest eccentricity e = 39.0625 mm</div></p>	01 01 01 01	04 (16)
Q.6	a)	<p>Attempt any <u>FOUR</u> of the following:</p> <p>State assumptions in theory of pure torsion. Assumptions:</p> <ol style="list-style-type: none"> 1. The shaft is straight having uniform circular cross section. 2. The shaft is homogeneous and isotropic. 3. Circular section remains circular even after twisting. 4. Plain section before twisting remains plain after twisting and do not twist or wrap. 5. A diameter in the section before deformation remains a diameter or straight line after deformation. 6. Stresses do not exceed the proportional limit. 7. Shaft is loaded by twisting couples in the planes that are perpendicular to the axis of the shaft. 8. Twist along the shaft is uniform. 	1/2 mark each	04



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.6	b)	<p>Find the torque that can be applied to a shaft of 100 mm in diameter, if the permissible angle of twist is 2.75° in a length of a 6 m. Take C = 80 kN/mm².</p>		
	Ans.	<p>Given data:</p> $\theta = 2.75^\circ = 2.75 \times \frac{\pi}{180} = 0.048 \text{ rad.}$ $d = 100 \text{ mm}$ $L = 6 \text{ m} = 6000 \text{ mm}$ $C = G = 80 \text{ kN/mm}^2 = 80 \times 10^3 \text{ N/mm}^2$ <p>Find: T</p> <p>From rigidity equation,</p> $\frac{T}{J} = \frac{G\theta}{L}$ $\frac{T}{\frac{\pi}{32} \times d^4} = \frac{G\theta}{L}$ $T = \frac{\pi \times d^4 \times G \times \theta}{32 \times L}$ $T = \frac{\pi \times 100^4 \times 80 \times 10^3 \times 0.048}{32 \times 6000}$ $T = 6282734.283 \text{ N-mm}$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">T = 6.282 kN-m</div>	<p>1/2</p> <p>1/2</p> <p>01</p> <p>02</p>	
	c)	<p>Find the power transmitted by a solid shaft of diameter 60 mm running at 220 rpm; if the permissible shear stress is 68 MPa. The maximum torque is likely to exceed the mean torque by 25%.</p>		
	Ans.	<p>Given:</p> $d = 60 \text{ mm}, N = 220 \text{ rpm}, \tau = 68 \text{ N/mm}^2$ $T_{\max} = 1.25 T_{\text{mean}}$ <p>Find: P = ?</p> $\frac{T_{\max}}{J} = \frac{\tau}{R}$ $T_{\max} = \left(\frac{\tau}{R} \right) J = \left(\frac{\tau}{\frac{d}{2}} \right) \frac{\pi}{32} d^4$	01	



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.6		$T_{\max} = \frac{\pi}{16} \times \tau \times d^3 = \frac{\pi}{16} \times 68 \times 60^3$ $T_{\max} = 2883.982 \times 10^3 \text{ N-mm}$ $T_{\max} = 1.25 T_{\text{mean}}$ $T_{\text{mean}} = \frac{T_{\max}}{1.25}$ $T_{\text{mean}} = \frac{2883.982 \times 10^3}{1.25} = 2307.1856 \times 10^3 \text{ N-mm}$ $T_{\text{mean}} = 2307.1856 \text{ N-m}$ <p>Power transmitted by shaft</p> $P = \frac{2\pi N T_{\text{mean}}}{60} = \frac{2\pi \times 220 \times 2307.1856}{60}$ $P = 53.153 \times 10^3 \text{ W}$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">P=53.153kW</div>	01	04
	d)	<p>Calculate the suitable diameter of the solid shaft to transmit 220 kW power at 150 rpm; if the permissible shear stress is 68 MPa.</p>	01	
	Ans.	<p>Given:</p> <p>Power = 220 kW = 220×10^3 W</p> <p>Speed N = 150 rpm</p> <p>Shear stress,</p> $f_s = 68 \text{ MPa} = 68 \text{ N/mm}^2$ <p>Find: D</p> <p>i) Using the relation,</p> $P = \frac{2\pi N T}{60} \text{ watts}$ $220 \times 10^3 = \frac{2 \times \pi \times 150 \times T}{60}$ $T = 14005.63499 \text{ N.m}$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">T = 14005.63499 × 10³ N-mm</div>	01	
		<p>ii) Using the relation,</p> $T = \frac{\pi}{16} \times f_s \times D^3$ $14005.63499 \times 10^3 = \frac{\pi}{16} \times 68 \times D^3$ $D = 101.604 \text{ mm}$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">Diameter of Shaft = 101.604 mm</div>	01	



Que. No.	Sub. Que.	Model Answers	Marks	Total Marks
Q.6.	e)	Find the torsional moment of resistance for a hollow circular shaft of 225 mm external diameter and 220 mm internal diameter, if the permissible shear is 60 MPa.		
	Ans.	Given: External Diameter $D = 225$ mm Internal Diameter $d = 220$ mm $\tau = 60$ MPa , Find: Torsional Moment or Resistance. $\frac{T}{J} = \frac{\tau}{R}$ $T_R = \left(\frac{\tau}{R}\right)J = \left(\frac{\tau}{\frac{d}{2}}\right)\frac{\pi}{32}(D^4 - d^4)$ $T_R = \left(\frac{60}{\frac{225}{2}}\right)\frac{\pi}{32}(225^4 - 220^4)$ $T_R = 11.536 \times 10^6 \text{ N-mm}$ $T_R = 11.536 \times 10^3 \text{ N-m}$	02	04
	f)	(i) Define - Section modulus. (ii) Define – Torsional stiffness.		
	Ans.	Section Modulus(Z): Section modulus is the ratio of M.I of the section about the Neutral Axis and the distance of the most extreme fiber from the Neutral axis. $Z = I/Y$ Torsional Stiffness: It is defined as the torque required per unit angle of twist. $\text{Torsional Stiffness} = T/\theta$	02	04
			02	