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### SUMMER-15 EXAMINATION Model Answer

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#### **Important Instructions to examiners:**

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more Importance (Not applicable for subject English and Communication Skills.
- 4) While assessing figures, examiner may give credit for principal components indicated in the figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
  - 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and model answer.
  - 6) In case of some questions credit may be given by judgement on part of examiner of relevant answer based on candidate's understanding.
  - 7) For programming language papers, credit may be given to any other program based on equivalent concept.

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Q No.	Answer	marks	Total marks
1A-a	Raoult's law: Raoult's law states that equilibrium partial pressure of a	1	2
	constituent at a given temperature is equal to the product of its vapour pressure		
	in pure state and its mol fraction in the liquid phase.		
	$P_{A} = P_{A}^{0} X_{A}$	1	
1A-b	Relationship between partial pressure and total pressure:		2
	For a gaseous mixture, total pressure is equal to the sum of partial pressures of	1	
	its components. This is called Dalton's law.		
	$P=P_1+P_2+P_3$	1	
	Where P is the total pressure of gas mixture and P <sub>1</sub> ,P <sub>2</sub> ,P <sub>3</sub> are partial pressures		
1A-c	Ideal Gas law:		2
	PV=nRT where P - pressure, V - volume, n- moles, K-absolute temperature	1	
	and R – universal gas constant		
	Value and unit of R is 8.314 KPa m <sup>3</sup> /kmol K	1	
1A-d		1	2
	→ Water evaporated X kg/hr		
	Feed F Kg/hr		
	$X_1$ % solid Evaporator		
	Thick liquor Y kg/hr		
	$\mathrm{X}_2$ % solid		
	Material balance for solids is		
	$X_1/100 *F = X_2/100 * Y$	1	



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1 A-e	Limiting component: It is the component or reactant which gets over first in a	1	2
	chemical reaction or it is the reactant which decides the extent of a reaction or it		
	is the reactant which is added in limited quantity.		
	% Conversion: (moles of limiting component reacted/ moles of limiting	1	
	reactant fed) * 100		
1A-f	Hess's law:	2	2
	It states that the heat involved in a chemical reaction is same whether the		
	reaction takes place in a single or in several steps.		
	A — → B ΔT1		
	$B \longrightarrow C \Delta T2$		
	$C \longrightarrow D \Delta T3$		
	$A \longrightarrow D \Delta T$		
	Then		
	$\Delta T = \Delta T 1 + \Delta T 2 + \Delta T 3$		
1B-a	Basis: 100 kmoles of air	1	6
	Average mol.wt of air= 0.79*28+0.21*32= 28.84	1	
	Density of air = P*Mav/ RT	1	
	At NTP, P= 101.325 KPa, R= 8.314, T=273 K	2	
	Density = $1.29 \text{ kg/m}^3$	1	
1B-b	Basis: 10000 Kg/hr of weak liquor	1	6
	→ Water evaporated X kg/hr		
	Feed10000 Kg/hr		
	10% NaOH Evaporator	1	
	Thick liquor Y kg/hr		
	55% NaOH		
	Overall balance is 10000= X+Y	1	



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Subject code :(17315) Page 4 of 21 Individual balance for caustic is 10/100 \* 10000 = 55/100 \* Y1 Y= 1818.18 & X= 8181.81 Kg/hr of water evaporated = **8181.81 Kg/hr** 2 Kg/hr of thick liquor obtained = 1818.18 Kg/hr 1B-c Basis: 10 kg C 6  $C+O_2 \rightarrow CO_2$ 1 Kmoles of C = 10/12 = 0.833 kmoles 1 Theoretical requirement of  $O_2 = 0.833$ Air is used 20% excess 1 Fed  $O_2 = 1.2 * 0.833 = 0.9996$ Fed  $N_2 = (79/21) * 0.9996 = 3.76$  $CO_2$  formed = 0.833 kmoles 1  $O_2$  unreacted = 0.9996-0.833 = 0.167 kmoles Composition of gases leaving combustion chamber: compound kmoles Mol% 0.167 3.51 2  $O_2$  $CO_2$ 0.833 17.5 3.76 78.99  $N_2$ 2-a **General Material Balance Procedure** 4 1) Assume Suitable Basis of calculation. 2) Adopt weight basis for without chemical reactions. 3) Draw Block diagram of the process of each operation with input and output stream. 4) In the block diagram drawn, indicate the information provided regarding input and output.



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	5) Search out u	ınknown and	ascertain them	and Calculate it	t by generating an	d	
	solving materia	ıl balance equ	ations.				
2-b	Basis: 100 kg gas mixture					1	
	component	weight	Mol.wt	kmoles	Mol %		
	$CO_2$	10	44	0.227	5.90		
	$N_2$	40	28	1.43	37.21	3	
	$O_2$	30	32	0.938	24.41		
	CH <sub>4</sub>	20	16	1.25	32.53		
2-c							
	10 kg 20 % NaCl, 30 % NaOH  mixture X Kg y % NaOH z% NaCl			1			
			, 25 % NaCl				
			5 Kg solution 2			1	
	Overall balance is $10+5 = X=15 \text{ Kg}$ Balance for NaOH is $30/100* 10 + 10/100*5 = y/100* 15$						
	y= $23.33 \%$	10H 1S 30/100	)* 10 + 10/100*	$5 = \frac{y}{100}$ * 15			
		Cl is 20/100*	10 + 25/100*5	- <sub>7</sub> /100* 15			
	z= 21.67 %	C1 13 20/100	10   23/100 3	- Z/100 13		1	
	Composition of water.	f resulting mi	xture is 23.33%	NaOH, 21.67 %	NaCl and 55%	1	



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=			
2-d			4
	→ Distillate X kg/hr	1	
	Feed 5000 Kg/hr 90% benzene		
	40% Benzene distillation		
	Bottom product Y kg/hr		
	10% benzene		
	Basis: 5000 kg/hr feed	1	
	Overall balance is $5000 = X+Y$		
	Balance for benzene is $0.4*5000 = 0.9 X + 0.1 Y$	1	
	Solving the equations $X=1875$ and $Y=3125$		
	Flow rate of top product = <b>1875 Kg/hr</b>	1	
	Flow rate of bottom product = 3125 Kg/hr		
2-е	Basis: 100kg methane fed		4
	Moles of methane fed = $100/16 = 6.25$ kmoles		
	$CH_4 + 2 O_2 \rightarrow CO_2 + 2H_2O$	1	
	Theoretical oxygen = 12.5 kmoles		
	Excess= 50 %		
	Fed $O_2$ = 18.75 kmoles		
	Fed $N_2 = 70.54 \text{ kmoles}$	1	
	% conversion is 40		
	Methane reacted = 2.5 kmoles		
	O <sub>2</sub> Reacted= 5		
	$O_2$ unreacted= $18.75-5 = 13.75$ kmoles		
	CO <sub>2</sub> formed= <b>2.5 kmoles</b>	1	
	$H_2O$ formed = <b>5 kmoles</b>		



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	CH <sub>4</sub> unreacted= 6.2	5-2.5 = <b>3.75</b> kmoles		
	compound	kmoles	Mol%	7
	$O_2$	13.75	14.39	1
	CO <sub>2</sub>	2.5	2.62	-
	H <sub>2</sub> O	5	5.23	
	CH <sub>4</sub>	3.75	3.93	
	$N_2$	70.54	73.83	
	Tota	l moles= 95.54 kmoles		_
2-f	$SO_2 + 0.5 O_2 \rightarrow SO_3$			
	Basis: 10 moles SO	<sub>2</sub> fed		1
	$SO_2$ fed = 10 kmole	es		
	Air fed = 100 kmole	es		
	$O_2$ Fed = 21 kmole	S		1
	Theoretical $O_2 = 5$ l	kmoles		1
	Excess $O_2 = [(Fed O)]$	O <sub>2</sub> - theoretical O <sub>2</sub> )/ theore	etical O <sub>2</sub> ]* 100	
	=( 21-5/	5)*100		1
	= 320 %	<b>o</b>		
3-a				1
			→ Water Evaporated	
	4000kg/hr			
	Feed 12% NaOH 12% NaCl	Evaporator	Thick Liquor 50% NaOH 1 % NaCl	



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76%	9 H <sub>2</sub> O 49% I	H <sub>2</sub> O	
	→ NaCl	. 1	
	Precipita	ted	
Basis: 4	0000 kg/hr of weak solution fed to the evaporator.		
Let X,Y, respectiv	Z be the kg/hr of water evaporated thick liquor & Nacl preciely.	ipitated	
Overall N	Material Balance :	1	
	$\Sigma$ Input stream = $\Sigma$ Output stream		
	40000 = X + Y + Z		
Material	balance of NaOH		
	NaOH in feed = NaOH in thick liquor		
	$0.12 \times 40000 = 0.5 \times Y$	2	
	$\therefore Y = 9600  \text{kg/hr}$		
		2	
Material	balance of NaCl NaCl in feed = NaCl in thick liquor + NaCl precipitated		
	$0.12 \times 40000 = 0.01 \times Y + Z$		
	4800 = 0.96 + Z		
	$\therefore Z = 4704 \frac{kg}{hr}$		
	nr	2	
We know	VX + Y + Z = 40000	2	
	$\therefore X = 25696  kg/hr$		
	w d area kg		
m1 : 1 1:	$\therefore Water\ evaporated = 25696 \frac{kg}{hr}$		
	uor obtained = <b>9600 kg/hr</b> stal precipitated = <b>4704 kg/hr</b>		
raciciy	star precipitated – 4704 kg/m		
)		1	
	$2S + 2O_2 \longrightarrow 2SO_2$	1	



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de .(17313)		rage 7 01 21
	$2 SO_2 + O_2 \longrightarrow 2 SO_3$	
	$2 SO_3 + 2 H_2O \longrightarrow 2 H_2 SO_4$	
	2S + 3 O2 + 2 H2O 2 H <sub>2</sub> SO <sub>4</sub>	
20ton/hr		
20000 kg/hr of	93.2 %	
$= 20000 \times 0.93$	32	1
= 18640 kg/hr		
2 x 98		
196 kg H <sub>2</sub> SO <sub>4</sub>	= 64 kg Sulphur	
	$H_2SO_4 = \frac{18640 \times 64}{196}$	2
	S = 6086.5  kg/hr	
	C 00 CF TDB	
	= <b>6.0865</b> T/hr	
	$O_{1} = \frac{18640 \times 96}{1}$	
	$O_2 = \frac{18640 \times 96}{196}$	
	- 0120 70 kg/bm	
	= 9129.79 kg/hr	2
	= <b>9.1297</b> T/hr	
	– 7.1271 1/m	



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			_
	$H_2O = \frac{18640 \times 36}{196}$		
	= 3423.6 kg/hr	2	
	= <b>3.4236 T/hr</b>		
3-с	Basis: 1 mole of liquid $CH_3COOH$ $C_{(s)} + O_2 \longrightarrow CO_2$ $\Delta H^o f = -393.3 \text{ KJ/mol}$	1	8
	$H_2(g) + \frac{1}{2}O_2 \longrightarrow H_2O \qquad \Delta H^0f H_2O = -285.8 \text{ KJ/mol}$		
	$CH_3COOH_{(1)} + 2O_2(g) \longrightarrow 2CO_2(g) + 2H_2O \qquad \Delta H^0c = -875 \text{ KJ/mol}$		
	$2Cs + 2H_2(S) + O_2(g) \longrightarrow CH_3COOH_{(I)} \qquad \Delta H^0f = ?$	2	
	$ \therefore \Delta H^{o}f = 2 \Delta H^{o}f + 2 \Delta H^{o}f H_{2} - \Delta H^{o}c $	3	
	= 2 (-393.3) + 2 (-285.8) - (-875)	2	
	= - 483.2 KJ/mol	2	
4-a	<b>Basis</b> : Gas mixture containing 0.274 kmol HCl,0.337 kmol N <sub>2</sub> ,0.089 kmol O <sub>2</sub> .		8
	Total moles of the gas mixture = $0.274 + 0.337 + 0.089 = 0.7$ kmol		
	Mole fraction of HCl $(X_{HCl}) = 0.274/0.7 = 0.399$		
	Mole fraction of $N_2$ ( $X_{N2}$ ) = 0.337/0.7 = 0.481	1	
	Mole fraction of $O_2$ ( $X_{O2}$ ) = 0.089/0.7 = 0.127		
	(i)Volume occupied by this mixture V = 3 atm = 303.975 kPa		



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PV = nRT	
$\therefore V = \frac{nRT}{P}$	
$= \frac{0.7 \times 8.3145 \times 303}{303.975}$	1
$= 5.80 \mathrm{m}^3$	1
(ii) Density of the Gaseous mixture $\mathbf{Mavg} = \boldsymbol{\Sigma} \ \mathbf{MiXi}$	
$= M_{HCl}.X_{HCl} + M_{N2}.X_{N2} + M_{O2}. X_{O2}$	
$= 36.5 \times 0.391 + 28 \times 0.481 + 32 \times 0.127$	1
∴ Mavg = 31.80	
∴ Density of the Gaseous mixture = Mavg / R x T	
$=\frac{303.975 \times 31.80}{8.3145 \times 303}$	1
$= 3.83 \text{ kg/m}^3$	
(iii) Partial pressure exerted by each component	
Total Pressure =303.975 Kpa	
Partial pressure of $HCl = P_{HCl} = X_{HCl}.P$	
$= 0.391 \text{ x} 303.975 = \mathbf{118.85kPa}$	
Partial pressure of $HCl = P_{N2} = X_{N2l}.P$	

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Partial pressure of HCl =	2			
	$= 0.127 \times 303.975 = 38.6$	60kPa		
$\begin{array}{c} \text{Composition} \\ \text{HCl} \\ \text{N}_2 \\ \text{O}_2 \end{array}$	Quantity in kg 10.001 9.436 2.848	Wt % 44.87 42.34 12.77		
Waste Acid 35% HNO <sub>3</sub> 35% H <sub>2</sub> SO <sub>4</sub> 30% H <sub>2</sub> O  Conc.HNO <sub>3</sub> 76%  Conc.H <sub>2</sub> SO <sub>4</sub>	Blending	Mixed Acid  → 42% HNO <sub>3</sub> 40% H <sub>2</sub> SO <sub>4</sub>	2	8
	Partial pressure of HCl =  (iv) Composition in Wt% $HCl = 0.274 \times 36.5 = 10$ $N_2 = 0.337 \times 28 = 9.436$ $O_2 = 0.089 \times 32 = 2.848$ Composition $HCl$ $N_2$ $O_2$ Basis: 1000 kg of desired m  Waste Acid $35\% \text{ HNO}_3$ $35\% \text{ H}_2\text{SO}_4$ $30\% \text{ H}_2\text{O}$ Conc.HNO <sub>3</sub> $76\%$ Conc.H <sub>2</sub> SO <sub>4</sub>	$= 0.481 \text{ x}303.975$ Partial pressure of HCl = $P_{O2}$ = $X_{O2}$ .P $= 0.127 \text{x}303.975 = \textbf{38.6}$ (iv) Composition in Wt% $HCl = 0.274 \text{ x} 36.5 = 10.001 \text{ kg}$ $N_2 = 0.337 \text{ x} 28 = 9.436 \text{ kg}$ $O_2 = 0.089 \text{ x} 32 = 2.848 \text{ kg}$ $\frac{\text{Composition}}{\text{N}_2} = \frac{9.436}{9.436}$ $O_2 = \frac{2.848}{22.285}$ $\frac{\text{Basis}: 1000 \text{ kg of desired mixed acid.}}{35\% \text{ H}_2\text{SO}_4}$ $\frac{30\% \text{ H}_2\text{O}}{30\% \text{ H}_2\text{O}}$ $\frac{\text{Conc.H}_2\text{SO}_4}{95\%}$ Blending	$= 0.481 \text{ x} 303.975 = \textbf{146.21kPa}$ Partial pressure of HCl = $P_{O2} = X_{O2}.P$ $= 0.127 \text{x} 303.975 = \textbf{38.60kPa}$ (iv) Composition in Wt% HCl = $0.274 \times 36.5 = 10.001 \text{ kg}$ N <sub>2</sub> = $0.337 \times 28 = 9.436 \text{ kg}$ O <sub>2</sub> = $0.089 \times 32 = 2.848 \text{ kg}$ $\frac{\text{Composition}  \text{Quantity in kg}  \text{Wt \%}}{\text{HCl}  10.001} \qquad \textbf{44.87}$ N <sub>2</sub> = $9.436 \times 42.34 \times 12.77 \times 12.22.285 \times 100 \times 1000 $	$= 0.481 \times 303.975 = \textbf{146.21kPa}$ Partial pressure of HCl = $P_{02}$ = $X_{02}$ .P $= 0.127 \times 303.975 = \textbf{38.60kPa}$ (iv) Composition in Wt% $\text{HCl} = 0.274 \times 36.5 = 10.001 \text{ kg}$ $N_2 = 0.337 \times 28 = 9.436 \text{ kg}$ $O_2 = 0.089 \times 32 = 2.848 \text{ kg}$ $\frac{\text{Composition}}{\text{NCl}} \qquad \frac{\text{Quantity in kg}}{\text{MCl}} \qquad \frac{\text{Wt \%}}{\text{42.34}}$ $O_2 \qquad 2.848 \qquad 12.77$ $22.285 \qquad 100$ $\text{Basis: } 1000 \text{ kg of desired mixed acid.}$ $\frac{\text{Waste Acid}}{35\% \text{ HNO}_3}$ $\frac{35\% \text{ HySO}_4}{30\% \text{ H}_2\text{O}}$ $\frac{\text{Conc.HNO}_3}{76\%} \qquad \frac{\text{Mixed Acid}}{40\% \text{ H}_2\text{SO}_4}$



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	$Y = kg \text{ of conc. } H_2SO_4$		
	$Z = kg$ of conc. $HNO_3$		
		1	
	. · . Overall Material Balance		
	1000 = X + Y + Z		
	(i)	1	
	Material Balance of H <sub>2</sub> SO <sub>4</sub>		
	0.35  x + 0.95  z = 0.4  x  1000		
	$Z = \frac{400 - 0.35x}{0.95}$		
	Z = 421.05 - 0.368  x		
		1	
	Material Balance of HNO <sub>3</sub>	1	
	0.35  x + 0.76  z = 0.42  x  1000		
	. $\cdot$ . $Z = \frac{420 - 0.35x}{0.76}$		
	Z = 552.63 - 0.460  x		
	Put value of Y & Z in eqn (i)		
	$. \cdot . \cdot 1000 = x + 421.05 - 0.368 \ x + 552.63 - 0.460 \ x$		
	26.32 = 0.172  x		
	x = 153.02  kg		
	Y = 421.05 - 0.368 (153.02)		



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	Y = 364.73 kg		
	Z = 552.63 - 0.460 (153.02)		
	= 482.24 kg		
	Waste acid required = 153.02 kg		
	conc. $H_2SO_4$ reqd. = <b>364.73 kg</b>	3	
	conc. $HNO_3$ reqd. = <b>482.24 kg</b>		
4-c	Basis: 100 kmol of HCl		8
	$4 \text{ HCl} + \text{ O}_2 \longrightarrow 2 \text{ Cl}_2 + \text{H}_2\text{O}$	1	
	30 % excess air required		
	80 % Conversion		
	. · . HCl reacted = 0.80 x 100 = 80 kmol		
	HCl unreacted = 20 kmol		
	4 kmol of HCl $\equiv$ 2 kmol of Cl <sub>2</sub> produced	1	
	. $^{\cdot}$ . $\text{Cl}_2$ produced from $\text{HCl} = 2/4 \times 80 = 40 \text{ kmol}$		
	$4 \text{ kmol of HCl} \equiv 1 \text{ kmol of O}_2$		
	. $\cdot$ . $O_2$ reacted = 1/4 x 80 = 20 kmol	1	



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But O <sub>2</sub> is calculated based	on reactant feed.		
. · . O <sub>2</sub> Therotical requirement	ent = $1/4 \times 100 = 25 \text{ km}$	nol	
As 30 % excess air is prov	ided.		1
O <sub>2</sub> in supp	lied air = 25 x (1 + $\frac{30}{100}$ )	= 32.5  kmol	
	= 2.5 - 20 =	12.5 kmol	
$O_2$ t	unreacted = $O_2$ in air - $O_2$	<sub>2</sub> reacted	1
	= 32.5 – 20 =	= 12.5 kmol	1
$N_2$ in su	pplied air = 79 /21 x 32.	5 = 122.26 kmol	
4 HC	Cl reacted $\equiv 2 \text{ kmol of H}$	120	
H2O	$produced = 2/4 \times 80 =$	40 kmol	1
. · . Composition of flue ga			
Vcl Component	Kmol	Mol %	
HCl	20	8.51	1
$Cl_2$	40	17.04	_
$O_2$	12.5	5.33	-
$N_2$	122.26	52.08	-
1		i	



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	224.76	100		
	234.76	100		
5-a	<b>Basis</b> : 100 Kg of Soyabean seeds		1	8
	It contains 18.6 kg oil ,69 kg solids and 12.4 kg			
	Let X be the Kg of cake obtained			
	Material balance of Solids:  Solids in seeds = Solids in cake		2	
	0.69 * 100 = 0.877 * X			
	X = 78.68  Kg			
	Material balance of Oil:  Oil in seeds = Oil in cake + Oil recove	red	2	
	$0.186*\ 100 = 0.008*\ 78.68 + \text{Oil recov}$	ered		
	18.6 = 0.6294 + Oil recovered			
	Oil recovered = $18.6 - 0.6294 = 17.97$ K	g		
	% recovery of Oil = * 100 Oil in Seeds		1	
	% recovery of Oil = 17.97 18.6		1	
	% recovery of Oil = 96.61 % ans.		1	
5-b	Basis: 100 Kmols of Water gas produced		1	8
	Volume % = Mole %			
	It contain H2= 55.4 Kmol			
	CO= 44 Kmol			
	CO2 = 0.6 Kmol		1	



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	Chemical Reactions		
	$C + H_2O \rightarrow CO + H_2$		
	$CO + H_2O \longrightarrow CO_2 + H_2$	2	
	From Reactions		
	$1 \text{ Katom C} \equiv 1 \text{ kmol CO}$		
	$\equiv 1 \text{ Kmol CO}_2$		
	Amount of C reacted = $1/1 *44 + 1/1 *0.6 = 44.6$ Katom		
	= 44.6 * 12 = 535.2  kg		
	Yield is 90% and coke contain 90% 'C'		
	Consumption of Coke = $535.2 / (0.9 * 0.9) = 660 \text{ kg}$	2	
	From the Reactions,		
	1 Kmol of $H_2O \equiv 1$ kmol $H_2$		
	Steam required = $1/1 * 55.4 = 55.4 \text{ kmol}$		
	Consumption of Steam = $55.4 *18 = 997.2 \text{ kg}$	2	
5-c	<b>Basis</b> : 100 Kg/hr of Water at 25 °C	1	8
	Q= Amount of heat required.		
	$Q = m \lambda v + m Cp (T_B - T)$	2	
	Where,		
	m = 100  kg/hr		
	Cp = 4.187  KJ/ Kg.K		
	Cp = 4.107 KJ/ Kg.K	2	
	$\lambda V = 2240 \text{ KJ/ Kg}$		
	$T = 25  {}^{\circ}C = 298  {}^{\circ}K$		
	$T_B = 100  {}^{\circ}\text{C} = 373  {}^{\circ}\text{K}$		
	Q = (100 * 2240) + (100 * 4.187 * (373-298))	2	



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	Q = 255402  KJ/hr				
	Q = 70.95  KJ/S	ans.		1	
a	<b>Basis</b> : 1 m3/hr gas	entering to absorpt	ion tower	1	
	Amount of Gas Ent	ering at 298 °K and	1 101.325 Kpa		
	n = PV/RT = (101.	325* 1)/(8.3145*	298) =0.040 kmol/hr	1	
	It contain				
	Solute gas = $(5/100)$	0)* 0.040 = 0.002  k	mol		
	Inert gas =(95/100)	* 0.040 = 0.038  km	ol		
	90% solute is abso	rb			
	Amount of solute a	1			
	Material balance of				
	Solute in Feed gas	s = Solute absorb +	Solute in outlet gas		
	0.002	= 0.0018 + Solute	in outlet gas		
	Solute in outlet gas	= 0.0002 kmol		1	
	Inert Balance				
	Inert in Inlet gas = Inert in Outlet gas				
	<b>Composition Outle</b>	et Gas :			
	Component	Kmol	Mol %		
	Solute gas	0.0002	0.52		
	Inert gas	0.038	99.47	2	
	Total	0.0382	100%		



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	$V = 0.934 \text{ m}^3 / \text{hr}$		
6-b	Basis: 5000 Kg/day MCA produced in small scale unit	1	8
	Amount Of MCA = 5000 Kg, Mol.Wt.Of MCA = 94.5		
	Amount Of $Cl_2 = 4536 \text{ Kg}$ , Mol.Wt.Of $Cl_2 = 71$		
	Amount Of DCA = 263 Kg, Mol.Wt.Of DCA = 129		
	Moles Of MCA = $5000/94.5 = 52.91$ Kmol	1	
	Moles Of $Cl_2 = 4536/71 = 63.89$ Kmol		
	Moles Of DCA = $263/129 = 2.03$ Kmol		
	Reactions		
	CH3COOH + Cl <sub>2</sub> → CH2ClCOOH +HCL (MCA)		
	CH2Cl COOH + Cl <sub>2</sub> → CH Cl <sub>2</sub> COOH +HCL (DCA)	1	
	Moles of MCA produced = Moles of MCA Charged = 52.91		
	From reaction 2,		
	1 Kmol of DCA $\equiv$ 1 kmol of MCA		
	2.03 Kmol of DCA $\equiv 1/1 * 2.03 \text{ kmol MCA}$		
	Moles of MCA reacted = 2.03 kmol		
	% Conversion of MCA = Moles of MCA reacted/ Moles of		
	MCA reacted	2	
	= (2.03 /52.91 ) * 100		
	% Conversion of MCA = 3.83 % ans.		
	From reaction 1		
	1 Kmol of MCA $\equiv$ 1 kmol of Cl <sub>2</sub>		
	52.91 Kmol of MCA $\equiv$ 52.91 kmol of Cl <sub>2</sub> reacted		
	From reaction 2,		
	1 Kmol of DCA $\equiv$ 1 kmol of Cl <sub>2</sub>		
	2.03 Kmol of DCA $\equiv$ 2.03 kmol of Cl <sub>2</sub> reacted		



### **SUMMER-15 EXAMINATION Model Answer**

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lower the temperature of a substance or mixture of substance.	1
(Cl <sub>2</sub> reacted for MCA / Cl <sub>2</sub> totally reacted )*100 = (52.91 / 54.94) * 100 % yield of MCA = 96.20%	1
= (52.91 / 54.94) * 100 % yield of MCA = 96.20% ans  6-c a) Sensible Heat: - Sensible heat is the heat that must be transferred to raise or lower the temperature of a substance or mixture of substance.  b) Latent Heat:- When matter undergoes a phase change, the enthalpy change associated with unit amount of matter at constant temperature and pressure is known as Latent Heat of phase change.  c) Heat of Reaction:-It is the enthalpy change resulting due to reaction wherein, reactants are fed in stoichiometric amounts and the reaction proceeds to completion.	1
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wherein, reactants are fed in stoichiometric amounts and the reaction proceeds to completion.	
to completion.	1
d) % Conversion: It is the ratio of amount of limiting reactant reacted to the	
	1
amount of limiting reactant totally charged. Express in percentage.	
1	1
system is known as Adiabatic process.	
f) Absorption of Gases: This the unit operation in which solute gas	
components from gas mixture is recovered or removal of gases with help of	1
suitable liquid solvent in which solute gas is absorbed.	



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