



MAHARASHTRA STATE BOARD OF TECHNICAL EDUCATION
(Autonomous)
(ISO/IEC - 27001 - 2005 Certified)

WINTER – 2019 EXAMINATION
MODEL ANSWER

Subject: Power System Operation and Control

Subject Code: 17643

Important Instructions to examiners:

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more Importance (Not applicable for subject English and Communication Skills).
- 4) While assessing figures, examiner may give credit for principal components indicated in the figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
- 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and model answer.
- 6) In case of some questions credit may be given by judgement on part of examiner of relevant answer based on candidate's understanding.
- 7) For programming language papers, credit may be given to any other program based on equivalent concept.

Q. No	Sub Q.N.	Answer	Marking Scheme									
1	(A) (a) Ans.	<p>Attempt any THREE: State the difference between 'Load bus' and 'Generator bus'. I Load Bus: At this bus power is injected or delivered to load. Hence real & reactive component of power is specified. At this bus voltage is allowed to vary within the permissible limit and phase angle 'δ' is not important from consumers point of view. This is also called as PQ bus. Power ejected from bus is considered as negative. II Generator bus: At this bus power generated is injected into the system. Hence the magnitude of voltage corresponding to its rating are specified from load flow solution and it is required to find out Q & S. This is also called as PV bus</p> <p style="text-align: center;">OR</p> <table border="1" style="width: 100%; border-collapse: collapse; margin-left: auto; margin-right: auto;"> <thead> <tr> <th style="width: 10%;">Sr. No.</th> <th style="width: 40%;">Load bus</th> <th style="width: 50%;">Generator Bus</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">1</td> <td>At this bus power is injected or delivered to load</td> <td>At this bus power generated is injected into the system</td> </tr> <tr> <td style="text-align: center;">2</td> <td>at this bus real & reactive</td> <td>At this bus magnitude of voltage</td> </tr> </tbody> </table>	Sr. No.	Load bus	Generator Bus	1	At this bus power is injected or delivered to load	At this bus power generated is injected into the system	2	at this bus real & reactive	At this bus magnitude of voltage	<p>12 4M</p> <p style="text-align: center;"><i>Any four points 1M each</i></p>
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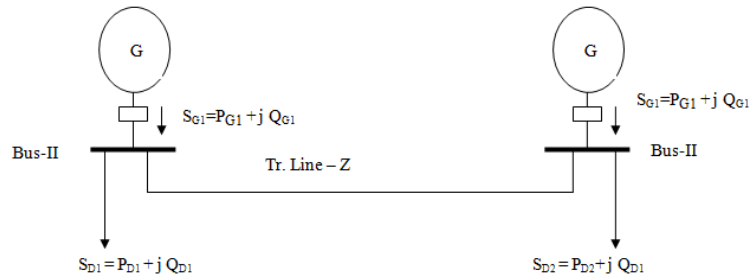
	(c) Ans.	State any two voltage control methods adopted in following areas: (i) Generating station (ii) Sub-stations Voltage control method (i) Generating station : 1. Automatic Voltage Control/Automatic Voltage regulator (AVR) 2. Excitation control by Tirril Regulator 3. Excitation control by Brown-Boveri Regulator (ii) Sub-stations: 1. By regulating transformers 2. By tap changing transformers. i. Off load tap changing Location – Distribution Substations, ii. On load tap changing Location- Intermediate Distribution Substations. 3. By tap changing Auto-transformers. 4. By booster transformers 5. By shunt capacitors Location – Distribution Substations, 6. By synchronous condenser location –	4M <i>Any 2 methods each 1M</i> <i>Any 2 methods each 1M</i>
	(d) Ans.	State the necessity of voltage control in power system operation. Necessity of voltage control in power system operation: 1. Maintains voltage profile 2. Better voltage regulation 3. Reduction reactive power flow 4. Reduction in losses as line current reduces 5. Improvement of P.F 6. Reduction in KVA demand charges 7. Decrease in KVA loading of generators	4M <i>Any four necessity 1M each</i>
1.	(B) (a) Ans.	Attempt any ONE: Derive $Y_{bus}V_{bus} = I_{bus}$ for a simple two-bus power system. Consider a simple two bus power system as shown in the fig.	06 6M



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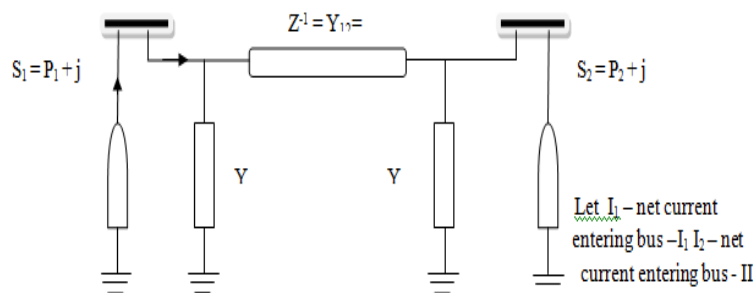
Let S_{G1} & S_{G2} be the power injected by the generators in bus – I and bus – II respectively. which was measured on the h. v. side of the transformers. Let S_{D1} & S_{D2} be the load demands on bus I & bus II respectively. Two buses are interconnected by a transmission line having Π equivalent ckt. Let V_1 and V_2 be the voltage at two buses I & II respectively.

Let S_1 & S_2 be the bus power which is defined as difference between generated power and load demand.

Hence,

$$\begin{aligned} S_1 &= S_{G1} - S_{D1} \\ &= (P_{G1} - P_{D1}) + j (Q_{G1} - Q_{D1}) \\ &= P_1 + j Q_1 \end{aligned}$$

This bus power can be considered as the power injected into the bus by a bus power source. Hence equivalent ckt. For the given system can be drawn as follow



i. e. bus current of bus - II i.e. bus current of bus - II

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		<p>Bus power S_1 can also be written as, $S_1 = V_1 I_1^*$ $I_1^* = S_1/V_1$ $I_1 = S_1^*/V_1^*$</p> <p>Where I_1 enters tr. Line from bus – I. By applying KCL at bus – I, we get $I_1 = V_1 Y + (V_1 - V_2) Y'$ We get $I_1 = S_1^*/V_1^* = V_1 Y + (V_1 - V_2) Y'$ ----- (1) $I_2 = S_2^*/V_2^* = V_2 Y + (V_2 - V_1) Y'$ ----- (2)</p> <p>The above two = o.s. can be simplified as $I_1 = V_1 (Y + Y') - Y' V_2$----- (3) $I_2 = -Y_1 Y' + (Y + Y') V_2$ ----- (3)</p> <p>Let $Y + Y' = Y_{11} = Y_{22}$ $-Y = Y_{12} = Y_{21}$</p> <p>Substituting in above equn, we get $I_1 = Y_{11} V_1 + Y_{12} V_2$ ----- (4) $I_2 = Y_{21} V_1 + Y_{22} V_2$ ----- (4)</p> <p>Above eq. 7 o.s. can be written in matrix form as, $\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} + \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$ ----- (5)</p> <p>i.e. $I_{bus} = Y_{bus} V_{bus}$ ----- (6)</p> <p>I_{bus} = bus current vector V_{bus} = bus voltage vector</p> <p>Y_{bus} – bus admittance matrix = $\begin{bmatrix} Y_{11} \\ Y_{12} \\ Y_{21} \\ Y_{22} \end{bmatrix}$</p>	<p><i>1M</i></p> <p><i>1M</i></p> <p><i>1M</i></p> <p><i>1M</i></p>
(b)	Ans.	<p>State and explain any three methods of improving transient stability condition in a power system.</p> <p>Following are methodsthat can be adopted for the improvement of transient stability condition of a power system: These techniques are classified as Traditional Technique and New Approaches</p>	6M



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	<p>i) Effects of Generator Design: A heavy machine has greater inertia and is more stable than a light machine. Modern machines are designed to get more power from smaller machines but this is undesirable from the stability point of view. In earlier days a large number of machines were employed to generate more power and this is also not desirable from stability point of view. A salient pole alternators operate at lower load angles and hence they are more preferred than cylindrical rotor generates from considerations of stability.</p> <p>ii) Increase of voltage: The amplitude of the power angle curve is directly proportional to the internal voltage of the machine. An increase in voltage increases the stability limit.</p> <p>iii) Reduction in transfer reactance: The amplitude of the power angle curve is inversely proportional to the transfer reactance. This reactance can be reduced by connecting more line in parallel. When two lines are connected in parallel and a fault occurs in one line then some power is transferred to healthy line (except when the fault is at receiving end or sending end bus. This transmission of power helps the stability of the system. Some features of the power system layout and business arrangement also help in improving stability. Use of bundled conductors helps in reducing line reactance and improving line stability. The compensation of line reactance by series capacitance is another effective method of improving stability.</p> <p>iv) Rapid fault clearing: By decreasing the fault cleaning angle (by using high speed breakers) stability can be improved.</p> <p>v) Automatic Reclosing: Most of the fault's on the transmission lines are of transient nature and are self-clearing. Modern circuit breakers are mostly of reclosing type. When a fault occurs, the faulted line is de-energized to suppress the fault and then the circuit breaker recloses, after a suitable time interval.</p> <p>vi) Quick valve opening action: During disturbance to generator more amount of power excess amount of steam is supply to turbine if turbine o/p is adjusted to get required generator o/p then system operate in equilibrium condition that means during disturbance turbine o/p has to be reduced by controlling flow of steam through valve hence now days electronic governors are used which operate valve electrically and controlled by electronics.</p> <p>vii) Application of braking resistors : whenever there is reduction sudden in load on generator without disturbing turbine i/p power then</p>	<p><i>Any 3 methods 2M each</i></p>
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		<p>generator can artificially loaded for this breaking R are used which will substituted loss of load /demand whenever fault occurs suitable control sy. Comes into action and connected R to generator terminals. A few cycle after clearance of fault same control sy. Disconnected braking and generator will continue to feed n/w.</p> <p>viii) Single pole switching: under large disturbance most of T.R line falls that occurs are 1Ø line to ground fault if ckt- breakers and protection scheme are properly arranged then only faulty line can be de – energized . Also most of fault under large disturbance occurs in transmission sy. Are transistaly teens after clearance of fault same phase line can put into service after certain time period depends on amount of fault current ckt voltage and wind velocity . it also not visible to operate system over- long period with 1Ø open hence some arrangement have to be make for tripping the entire 3Ø line if fault fault remain for longer period.</p> <p>ix) Fast acting automatic voltage regulator: whenever fault occurs insy. Voltage at all buses in system reduces the voltage at generator bus can controlled and maintain by excitation generator sy. For this purpose automatic voltage regulators is used similarly voltage at difference buses also reduce due to sault current and drop in voltage across transmission line heance in modern power system voltage control equipment are used at specific buses in system the modern voltage regulators respond rapidly(0.5-1.5 cycle).</p>	
2.	(a) Ans.	<p>Attempt any FOUR: State the effect of change in frequency on various consumers and utilities. Effect of change in frequency on various consumers:</p> <ol style="list-style-type: none">1) In most of the industries, Induction motor is used as common drive, which runs at speed that is directly related with frequency. (N= 120f/p) variation in frequency affects the quality of the product and rate of production.2) Induction motor used as common a.c. drives though has rigid construction but due to variation in supply frequency, life of induction motor reduces by 500 Hrs. They are not sensitive for small variation in the supply frequency. i.e. of the order of 50 ± 2 Hz.3) In railway stations, the electric chokes are driven by single-phase synchronous motor, The speed of the synchronous motor depends	16 4M <i>Any 4 effect 1M each</i>



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		<p>on supply frequency directly. Hence it needs constant frequency supply for all 24 Hrs. of the day. If frequency falls by 1 hr , then clock falls back by 15 min. & it takes no. of hours to reduce the error to zero.</p> <p>4) In some industries such as the textiles rubber, plastic & paper require frequency constant or to a tolerance of ± 0.25 per min.</p> <p>5) Electric gear systems used in industries requires the frequency 49.5 Hz to 50.5 Hz range.</p> <p>6)</p>	
(b) Ans.	<p>List out the advantages of reactive power compensation in power system.</p> <p>Advantage of reactive power compensation</p> <ol style="list-style-type: none">1. Reduction in reactive component of circuit current2. Maintenance of voltage profile within limits3. Reduction of Copper losses in the system due to reduction of current.4. Reduction in investment in the system per kW of load supplied5. Decrease in KVA loading of generators and circuits. This decrease in KVA loading may relieve an overload condition or release capacity for additional load growth.6. Improvement in p.f. of generators.7. Reduction in KVA demand charges for large consumers8. Overall improvement in system efficiency.	12	<p><i>Any four advantages 1M each</i></p>
(c) Ans.	<p>List out the data required for Load flow studies.</p> <ul style="list-style-type: none">• Single line diagram of a power system.• Transmission line data -<ol style="list-style-type: none">(a) Line parameters – Series impedance (z) in per unit shunt admittance (y) thermal limits of the line.(b) Length of the line.(c) Identification of each line and its II equ. Ckt.• Transformer ratings, impedance and tap setting are required. Quite often it may be necessary to adjust voltages on one or both sides of the transformers to maintain the potential levels at the neighboring buses within specified limits. For achieving this, auto and double winding transformers with provision for tap changing on h. v. side or used so as to facilitate smoother control.• At certain buses, static capacitors are used for voltage level improvement their admittance value should be clearly specified.• Some of lines may be tuned for the purpose of voltage	4M	<p><i>Any four points 1M each</i></p>



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		<p>stabilization, by using shunt reactors or series capacitors. Their values should be made available.</p> <ul style="list-style-type: none">Depending upon no. of buses in the system bus data should be made available : - <table border="1"><thead><tr><th>Type of bus</th><th>No of buses</th><th>Bus data</th></tr></thead><tbody><tr><td>Generator bus</td><td></td><td>P, (V)</td></tr><tr><td>Load bus</td><td></td><td>P, Q</td></tr></tbody></table> <ul style="list-style-type: none">If the load flow study is to be carried out for a specified load demand then the most effective manner in which generation can be scheduled at the various buses so as to ensure the desired voltage profile. A no. of load flow solutions is possible for different sets of control parameters. <p style="text-align: center;">OR</p> <p>Following Data are required for load flow analysis:</p> <ol style="list-style-type: none">System data: It includes: Single line diagram system of a power, number of buses-n, number of PV buses, number of loads, number of transmission lines, number of transformers, number of shunt elements, the slack bus number, voltage magnitude of slack bus (angle is generally taken as 0°), tolerance limit, base MVA, and maximum permissible number of iterations.Generator data: No. of generating stations connected in the system ready to generate the required amount of power and their time duration should be available. Each generator's rating, maximum & minimum limits of generation, their characteristics, and excitation control details are made available.Transmission line data - For every transmission line connected between buses i and k the data includes the starting bus number i, ending bus number k,<ul style="list-style-type: none">Line parameters – resistance of the line, reactance of the line and the half line charging admittance. Series impedance (z) in per unit, shunt admittance (Y) in per units,Thermal limits of the line.Length of the line.Identification of each line and its 'π' equivalent circuit.Transformer data: Type of transformer such as distribution	Type of bus	No of buses	Bus data	Generator bus		P, (V)	Load bus		P, Q	
Type of bus	No of buses	Bus data										
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		<p>transformer / power transformer, auto-transformer, tap-changing transformer (on-line or ff-line). Also ratings, % impedance and tap setting points, tap setting on HV /LV /both sides are required. (Quite often it may be necessary to adjust voltages on one or both sides of the transformers to maintain the potential levels at the neighboring buses within specified limits. For achieving this, auto and double winding transformers with provision for tap changing on H. V. side or used so as to facilitate smoother control. For every transformer connected between buses i and k the data to be given includes: the starting bus number i, ending bus number k, resistance of the transformer, reactance of the transformer, and the off nominal turns-ratio.</p> <p>5. Bus data: Depending upon no. of buses in the system, bus data should be made available.</p> <table border="1" style="width: 100%; border-collapse: collapse; margin: 10px 0;"> <thead> <tr> <th style="text-align: center;">Type of bus</th> <th style="text-align: center;">Bus data</th> <th style="text-align: center;">No of buses</th> <th style="text-align: center;">For each Bus</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Generat or bus</td> <td style="text-align: center;">P, (V)</td> <td></td> <td>P_{Gi}, V_i, minimum and maximum reactive power limit ($Q_{i,min}$, $Q_{i,max}$).</td> </tr> <tr> <td style="text-align: center;">Load bus</td> <td style="text-align: center;">P, Q</td> <td></td> <td>active power demand P_{Di}, and the reactive power demand Q_{Di}.</td> </tr> <tr> <td style="text-align: center;">Slack bus</td> <td style="text-align: center;">V, δ</td> <td></td> <td>Generator ratings which is assume to be connected to slack bus</td> </tr> <tr> <td style="text-align: center;">Voltage control bus</td> <td style="text-align: center;">P Q V</td> <td></td> <td>Voltage control equipment used and its rating, max. & min. limits</td> </tr> </tbody> </table> <p>6. Some of lines may be tuned with reactive compensating equipments, for stabilizing the voltage level. Their ratings and setting values should be made available.</p> <p>7. If the load flows study is to be carried out for a specific load demand, then the most effective manner in which generation can be scheduled at the various buses by ensuring the desired voltage profile. A no. of load flow solutions is possible for different sets of control parameters. It is therefore necessary to define and objective of load flow analysis.</p>	Type of bus	Bus data	No of buses	For each Bus	Generat or bus	P, (V)		P_{Gi} , V_i , minimum and maximum reactive power limit ($Q_{i,min}$, $Q_{i,max}$).	Load bus	P, Q		active power demand P_{Di} , and the reactive power demand Q_{Di} .	Slack bus	V, δ		Generator ratings which is assume to be connected to slack bus	Voltage control bus	P Q V		Voltage control equipment used and its rating, max. & min. limits	
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(d) Ans.	<p>State the characteristics of Y_{bus} matrix.</p> <p style="text-align: center;">The admittance matrix is $Y_{bus} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} \\ Y_{21} & Y_{22} & Y_{23} \\ Y_{31} & Y_{32} & Y_{33} \end{bmatrix}$</p> <div style="text-align: center; background-color: #f0f0f0; padding: 10px; margin: 10px 0;"> <p>Where,</p> $Y_{11} = Y_{11} + Y_{12} + Y_{13} \quad \&$ $Y_{22} = Y_{21} + Y_{22} + Y_{23} \quad \&$ $Y_{33} = Y_{31} + Y_{32} + Y_{33}.$ <p>Also,</p> $Y_{12} = Y_{21} = -Y_{12} = -Y_{21} \quad \&$ $Y_{13} = Y_{31} = -Y_{13} = -Y_{31} \quad \&$ $Y_{23} = Y_{32} = -Y_{23} = -Y_{32}.$ </div> <p>Characteristics of Y_{bus} matrix:</p> <ol style="list-style-type: none"> 1) Y_{bus} is a symmetrical matrix “n x n” matrix. 2) All diagonal elements Y_{ii} represent “self admittances” of bus “I”. 3) All off diagonal elements Y_{ij} represents mutual admittance between bus “I” bus “j”. 4) With reference to mutual admittance $Y_{ij} = Y_{ji}$.e. $Y_{12} = Y_{21}$, $Y_{13} = Y_{31}$ Hence it is a symmetrical matrix. 5) Any element in the matrix „zero“ indicates that there is not to line between those buses. $Y_{21} = Y_{12} = 0$ no tr. line between bus I bus II or outage of tr. line $Y_{ik} = Y_{ki} = 0$ if i k between but I bus II i k are not connected. 6) $Y_{bus} = (Z_{bus})^{-1}$ where Z_{bus} – bus impedance matrix. 7) All elements are complex numbers. 8) Self admittances are defined as $Y_{11} = Y_{11} + Y_{12} + Y_{13}$ Where Y_{11} – line changing admittance Y_{12}, Y_{13} – line admittances Y_{11} = sum of line changing admittance and total line admittances connected to a bus. 9) Mutual admittances are defined as $Y_{12} = -Y_{12} = -Y_{21} = Y_{21}$ $Y_{13} = -Y_{13} = Y_{31}$ i.e. mutual admittance is negative of line admittance between two buses. 	4M
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		10) All mutual admittances are negative complex numbers.	
	<p>(e)</p> <p>Ans.</p>	<p>With reference to power system define-</p> <p>(i) Steady state stability (ii) Steady state stability limit (iii) Transient state stability (iv) Transient state stability limit.</p> <p>(i) Steady state stability: When the power system has capacity to regain and maintain equilibrium condition (synchronous speed) after a small slow disturbance such as load variation or changes in load condition occurs, then the power system is said to be in steady state stability condition.</p> <p>(ii) Steady State stability limit: It is defined as max power which can flow through point in the system without causing loss of stability, when system experiences a small disturbance.</p> <p>(iii) Transient stability: Transient stability is the ability of the power system to regain or maintain equilibrium conditions after experiencing a large sudden disturbance.</p> <p>(iv) Transient state stability limit: It refers to max possible flow of power through a point without loss of stability when system experiences a large sudden disturbance.</p>	<p>4M</p> <p><i>Each definition 1M</i></p>
	<p>(f)</p> <p>Ans.</p>	<p>State and explain ‘dynamic state stability’ and ‘overall stability’ of a power system.</p> <p>Dynamic state stability: It is the condition of the power system which lies between the study state stability and transient state stability.</p> <p>Dynamic stability of a system denotes the artificial stability given to an inherently unstable system by automatic controlled means. It is generally concerned to small disturbances lasting for about 10 to 30 seconds.</p> <p>When a generator feeding power into a large network is subjected to a small disturbance, the dynamic response of the generator rotor with respect to the system is oscillatory with, in general, relatively light damping. This produces oscillatory variations in the magnitudes of the generator voltage, currents, power and torque. Under such circumstances it is often useful to consider the influence of</p>	<p>4M</p> <p><i>Dynamic state stability 2M</i></p>

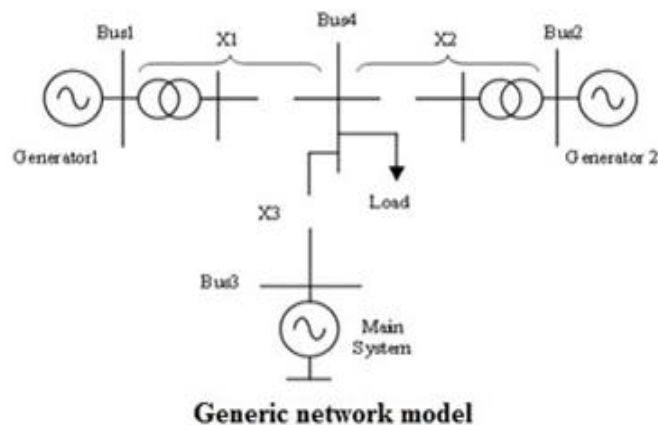


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controllers and system elements on performance in terms of their influence on synchronising power and damping power. Oscillations in power (or torque) resulting from the disturbance are considered to be expressible in terms of two components. One is the component of power oscillations that is in phase with rotor angle oscillations; this is termed the synchronising power component. The other is the component in phase with rotor speed oscillations; this is termed the damping power component.



A controller that increases the magnitude of the power component in phase with rotor speed, i.e. the damping power, will improve the damping of the system oscillations. Any increase produced in the synchronising power component indicates that changes in rotor angle produce greater changes in the restoring torque on the generator shaft, which helps ensure that the generator remains in synchronism with the system being supplied. The term synchronising power (or torque) is, in addition, often applied to large disturbance situations, such as behaviour following three-phase system faults. Here the term simply applies to the load power (or load torque) developed, which is predominantly related to the swing in rotor angle. This load torque acts on the rotor and in such a direction as to return it to the final equilibrium value of rotor angle where the system is again in a steady condition and in synchronism with the system being supplied.

Over all stability: It is the stability of a power system when synchronism of one of working generator has been lost. The normal



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		operating condition can be reestablished without disconnection of major elements. Modern power system uses automatic control devices and therefore it is to be tested for its ability to remain in synchronism under steady state as well as transient conditions. Both prior to and after the disturbance. Such operating condition of system is called as Over all stability.	Overall stability 2M
3.	(a) Ans.	<p>Attempt any FOUR: State and explain concept of reactive power compensation. State: This method of generating the reactive power locally to meet the demand instead of generating at generating station and meeting the consumers demand is called as reactive power compensation:</p> <p>The main objective of the utilities is to satisfy the consumers with its power demand. To meet the consumer’s reactive power demands, if the same power is generated at generating stations & feed to the consumer, it will cause voltage drop in line. This will result into reduction of transmission efficiency and the cost of power transmission increases. Instead of this is we generate power locally near the load centers& feed it to consumers to his satisfaction the performance of power system will not affect & cost of power transmission also will not increase.</p> <p>Reactive power generating equipments are located near the load centers which will help to meet the reactive power demand of consumers to his satisfaction. These also help to control the voltage levels in the system. The methods used for this is also called as “Reactive Power Compensation “. And the equipment used is called as “reactive power compensating equipment”. Reactive power compensating equipment can be employed either at load level, substation level, or at transmission level.</p>	16 4M State 1M Explanation 3M
	(b) Ans.	<p>State the difference between shunt compensation and series compensation refer to reactive power compensation.</p>	4M



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		<p>V_1, V_2, \dots, V_n are the bus voltages $\delta_1, \delta_2, \dots$ are load angles with reference to bus-1, bus-2 and so on. Y_{11}, Y_{22}, \dots are self admittance with reference to bus-1, bus-2 and so on. Y_{12}, Y_{21}, \dots are Mutual admittance with reference to bus-1, bus-2 and so on S_1, S_2, \dots complex power at bus-1, bus-2. P_1, P_2, \dots Real power at bus-1, bus-2. Q_1, Q_2, \dots Reactive power at bus-1, bus-2.</p>	2M
	<p>(d) Ans.</p>	<p>List out the informations that can be collected from load flow studies.</p> <ol style="list-style-type: none"> (1) We get MW and MVAR flow in the various parts of the system network. (2) We get information about voltages at various buses in the system. (3) We get information about optional load distribution. (4) Impact of any change in generation (increase or decrease) on the system. (5) Influence of any modification or extension of the existing circuits on the system loading. (6) It also gives information for choice of appropriate rating and tap-setting of the power transformer in the system. (7) Influence of any change in conductor size and system voltage level on power flow. 	<p>4M</p> <p style="text-align: right;"><i>Any four points 1M each</i></p>
	<p>(e) Ans.</p>	<p>Derive the equation for maximum power flow under steady state condition, considering a simple two bus power system.</p> <p>Consider a simple power system with less transmission line as shown in figure.</p> <div style="text-align: center;"> </div> <p>Power transmitted from S.E. to R.F. is $S = V_S I$</p> <p>Where $I = \frac{V_S - V_R}{jX} = V_S$</p>	<p>4M</p> <p style="text-align: right;">1M</p>



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		$P_{\max} = \frac{V_S V_R}{X}$ <p>This is the maximum power flow for steady state stability.</p>	
<p>(f)</p> <p>Ans.</p>	<p>Draw and explain power angle diagram neglecting losses in the system.</p> <p><u>WITHOUT LOSSES.</u></p> <div style="text-align: center;"> </div> <p>The power angle equation of a two machine system model can be written as</p> $P = \frac{V_1 V_2}{X} \sin \delta$ <p>Where $V_1 \angle \delta$ $V_2 \angle 0$ are Bus voltages</p> <p>δ – Load angle X – transfer reactance of line.</p> <p>Now locus power ‘P’ with respect to load angle ‘S’ is called power angle curve. For constant values of V_1 V_2 and for same transfer line x constant.</p> <p>Then $P \propto \sin \delta$ when δ is positive i.e. $0 < \delta < 180^\circ$ the power P is positive. That means power flows from generator to load. For positive values of δ P is negative i.e. power flows from load to generator.</p> <p>In system power always flows from generator to load in normal operating condition.</p> <p>When $\delta = 0$ $P = 0$ i.e. power flow</p>	<p style="text-align: right;">4M</p> <p style="text-align: right;">Diagram 2M</p> <p style="text-align: right;">Explanation 2M</p>	



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		<p>As δ increases power generation also increases When $\delta = 90^\circ$ $\sin \delta = 1$</p> $\therefore P = P_{\max} = \frac{V_1 \cdot V_2}{X}$ <p>For any value of P we have 2 points on the diagram 'A' and 'B' say P is constant but rotor speed due to some reason has momentarily increased so the rotor angle δ to $(\delta + \Delta\delta)$ which corresponds to 'A'. So the corresponding output power is $(P + \Delta P)$. Now the imbalance occurs between generation α consumption and as a result rotor speed decreases and settle down to 'δ' after certain oscillations. So 'A' is stable operating power. If 'B' is stable operating point then small increase by $\Delta\delta$ would shift B to B¹. Hence power output decreases and is less than P_0. Now the rotor will experience accelerating power but the rotor output decrease further and 'δ' will continue to increase few there and 'δ' will not be restored \therefore B is in unstable condition.</p> <p>At point A \rightarrow $\delta \delta \rightarrow \Delta\delta$ then $P \rightarrow \Delta P$</p> <p>As rotor output \uparrow \rightarrow rotor speed \downarrow \rightarrow $\delta \downarrow$</p> <p>At point B \rightarrow $\delta \delta \rightarrow \Delta\delta$ then $P \rightarrow \Delta P$</p> <p>Rotor output \downarrow \rightarrow rotor speed $\downarrow\downarrow$ \rightarrow $\delta \downarrow$ unstable</p> <p>$\therefore 0 \leq \delta \leq 90^\circ$ -----stable region $90^\circ \leq \delta \leq 180^\circ$ -----unstable region</p> <p>Practically system operates for $30^\circ < \delta < 45^\circ$.</p>	
4.	<p>(A) (a) Ans.</p>	<p>Attempt any THREE: State and explain following equations refer to power system. (i) Bus loading equation (ii) Line flow equation</p>	<p>12 4M</p>



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		<p>Similarly power flows from j to k is</p> $P_{j k} - jQ_{j k} = V_j^* I_{jk} = V_j^* (V_j - V_k) y^l + V_j^* V_j Y/2$ <p>The above two equations are called as “Line flow equation”. The algebraic sum of power expressed by above equations gives power loss in the transmission line k – j.</p>	
	<p>(b) Ans.</p>	<p>State the advantages of Y_{bus} matrix in load flow studies. <i>(Note: Any other advantages shall be considered)</i></p> <ol style="list-style-type: none"> 1. Data preparation for LFs is simple. 2. Its information of Y_{bus} matrix for any system. 3. Modification of Y_{bus} matrix due outage of transmission lines or transformer is easy. 4. Y_{bus} is a sparse matrix (i.e. most of its elements are zero). ∴ the computer memory requirements are less. For a large power system more than 90% of its off. Diagonal elements are zero. This is due to the fact that in power system network each bus is connected to not more than 3 buses in general αy_{pq} exists only if transmission line links bus p αq. 	<p>4M</p> <p><i>Any four advantages 1M each</i></p>
	<p>(c) Ans.</p>	<p>Write ‘Swing equation’ referred to power system and define it’s parameters.</p> $M \frac{d^2 \delta}{dt^2} = P_a = P_m - P_e$ <p>wherem = angular momentum, P_m = mechanical power input, P_e = electrical power output, P_a = accelerating power, δ = angular displacement of rotor</p>	<p>4M</p> <p><i>Equation 3M</i></p> <p><i>Meaning of each term 1M</i></p>



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	<p>(d)</p> <p>Ans.</p>	<p>List out the methods of improving transient stability in a power system.</p> <p>There are main two methods: Traditional Technique and New Approaches</p> <table style="width: 100%; border: none;"> <tr> <td style="width: 50%; vertical-align: top;"> <p>Traditional Technique:</p> <ul style="list-style-type: none"> i) Effect of generator design. ii) Increase of voltage iii) Reduction in transfer reactance iv) Rapid fault clearing v) Automatic reclosing </td> <td style="width: 50%; vertical-align: top;"> <p>New Approaches:</p> <ul style="list-style-type: none"> i) Quick valve opening action. ii) Application of braking resistors iii) Single pole switching iv) Fast acting automatic voltage regulator </td> </tr> </table>	<p>Traditional Technique:</p> <ul style="list-style-type: none"> i) Effect of generator design. ii) Increase of voltage iii) Reduction in transfer reactance iv) Rapid fault clearing v) Automatic reclosing 	<p>New Approaches:</p> <ul style="list-style-type: none"> i) Quick valve opening action. ii) Application of braking resistors iii) Single pole switching iv) Fast acting automatic voltage regulator 	<p>4M</p> <p><i>Any 4 methods 1M for each</i></p>
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<p>4.</p>	<p>(B)</p> <p>(a)</p> <p>Ans.</p>	<p>Attempt any ONE:</p> <p>Draw neat labeled schematic diagram of turbo generator with load-frequency control and voltage control.</p> <div style="border: 1px solid black; padding: 10px; text-align: center;"> </div>	<p>06</p> <p>6M</p> <p><i>5M for components and 1M for labeling</i></p>		
	<p>(b)</p> <p>Ans.</p>	<p>List out the information of Load Dispatch Centre (LDC). <i>(Note: Functions of any type of LDC shall be considered).</i></p> <p>Functions of National Load Dispatch Centre:</p> <ol style="list-style-type: none"> 1. Supervision over the RLDCs. 2. Scheduling and dispatch of electricity over inter-regional links in accordance with Grid standards specified by the Authority and Grid Code specified by the Central Commission in coordination with RLDCs. 	<p>6M</p>		



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		<ol style="list-style-type: none"> 3. Coordination with RLDCs for achieving maximum economy and efficiency in operation of National Grid. 4. Monitoring of operations and grid security of the National Grid. 5. Supervision and control over the inter regional links as may be required for ensuring stability of the power system under its control. 6. Co-ordination with Regional Power Committees for regional outage schedule in the national perspective to ensure optimum utilization of power resources. 7. Coordination with RLDCs for the energy accounting of inter-regional exchange of power. 8. Coordination for restoration of synchronous operation of National Grid with RLDCs. 9. Co-ordination for trans-national exchange of Powers. 10. Providing operational feed-back for National Grid planning to the Authority and the Central Transmission Utility. 11. Levy and collection of such fee and charges from the Generating Companies or the licensees involved in the power system as may be specified by the Central Commission. 12. Dissemination of information relating to operations of transmission system in accordance with directions or regulations issued by the Central Commission and the Central Government from time to time. 	<p><i>Any 6 1M each</i></p>																
5.	(a)	<p>Attempt any FOUR: Develop Y_{bus} matrix for a 3bus system with following details:</p> <table border="1" style="margin-left: auto; margin-right: auto; border-collapse: collapse;"> <thead> <tr> <th style="padding: 5px;">Bus Code</th> <th style="padding: 5px;">Line impedance (Pu)</th> <th style="padding: 5px;">Bus Code</th> <th style="padding: 5px;">Line Charging admittance (Pu)</th> </tr> </thead> <tbody> <tr> <td style="padding: 5px;">1 – 2</td> <td style="padding: 5px;">0.085 + j0.32</td> <td style="padding: 5px;">1</td> <td style="padding: 5px;">j0.01</td> </tr> <tr> <td style="padding: 5px;">2 – 3</td> <td style="padding: 5px;">0.045 + j0.06</td> <td style="padding: 5px;">2</td> <td style="padding: 5px;">j0.03</td> </tr> <tr> <td style="padding: 5px;">1 – 3</td> <td style="padding: 5px;">0.055 + j0.08</td> <td style="padding: 5px;">3</td> <td style="padding: 5px;">j-0.00</td> </tr> </tbody> </table>	Bus Code	Line impedance (Pu)	Bus Code	Line Charging admittance (Pu)	1 – 2	0.085 + j0.32	1	j0.01	2 – 3	0.045 + j0.06	2	j0.03	1 – 3	0.055 + j0.08	3	j-0.00	<p>16 4M</p>
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	Ans.	<p>$Z_{12} = 0.085 + j0.32$ $Z_{23} = 0.045 + j0.06$ $Z_{13} = 0.055 + j0.08$</p> <p>Calculation of mutual admittances....</p>																	



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	$y_{12} = \frac{1}{z_{12}} = \frac{1}{0.085 + j0.32} = \frac{1}{0.33 \angle 83.47} = \frac{1}{0.33 \angle 75.12}$ $= 3.03 \angle 75.12$ $y_{12} = 0.77 - j2.9$ $y_{23} = \frac{1}{z_{23}} = \frac{1}{0.045 + j0.06} = \frac{1}{0.075 \angle 53.13} = 13.33 \angle 53.13$ $y_{23} = 7.99 - j10.66$ $y_{13} = \frac{1}{0.055 + j0.08} = \frac{1}{0.097 \angle 55.49} = 10.309 \angle -55.49$ $y_{13} = 5.840 - j8.49$ $y_{12} = y_{21} - y_{12} = -y_{21}$ $= - (0.77 - j0.9)$ $y_{13} = y_{31} - y_{13} = -y_{31}$ $= - (5.840 - j8.49)$ $y_{23} = y_{30} - y_{23} = -y_{32}$ $= - (7.88 - j10.66)$ <p>Calculation of self-admittances....</p> $y_{11} = y_{11} + y_{12} + y_{13}$ $= j0.01 + (0.77 - j2.9) + (5.840 - j8.49)$	<p><i>1½M</i></p> <p><i>1½M</i></p>
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	$= 6.61 - j11.38$ $Y_{22} = Y_{21} + Y_{22} + Y_{23}$ $= 0.77 - j2.9 + j0.03 + (7.99 - j10.66)$ $= 8.76 - j13.53$ $Y_{33} = Y_{31} + Y_{32} + Y_{33}$ $= 5.840 - j8.49 + 7.99 - j10.66 + (-j0.01)$ $= 13.83 - j19.16$ <p>\therefore Required Y_{bus} is</p> $Y_{bus} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} \\ Y_{21} & Y_{22} & Y_{23} \\ Y_{31} & Y_{32} & Y_{33} \end{bmatrix}$ $= \begin{bmatrix} 6.61 - j11.38 & -(0.77 - j2.9) & -(5.840 - j8.49) \\ -(0.77 - j2.9) & (8.76 - j13.53) & -(7.99 - j10.66) \\ -(5.846 - j8.49) & -(7.99 - j10.66) & -(13.83 - j19.16) \end{bmatrix}$ $Y_{bus} = \begin{bmatrix} 6.61 - j11.38 & -0.77 + j2.9 & -5.840 - j8.49 \\ -0.77 - j2.9) & 8.76 - j13.53 & -7.99 + j10.66 \\ -5.846 - j8.49 & -7.99 - j10.66) & 13.83 - j19.16 \end{bmatrix}$	<i>1M</i>
(b) Ans.	With the help of diagram explain voltage control by reactive power injection method. Voltage control by reactive power injection method:	4M



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			<p><i>Diagram</i> 1M</p>
		<ol style="list-style-type: none"> 1. To keep the receiving end voltage of specified value V_{SR} a fixed amount of VARs Q_R^S must be drawn from the line. 2. To accomplish this under conditions of a varying VAR demand. Q_D a local VAR generator must be used as shown in figure. 3. The VAR balance equation at the receiving end is now, $Q_R^S + Q_C = Q_D$ 5. Fluctuations is an are absorbed by the load VAR generator Q_C such that the VARs drawn from the line remain fixed at Q_R^S 6. The receiving end voltage would thus remain fixed at V_R^S. Local VAR compensation can, in fact be made automatic by using the signal from the VAR meter installed at the receiving end of the line. 	<p><i>3 m for</i> explanation <i>ion</i></p>
	<p>(c)</p> <p>Ans.</p>	<p>State the functions of following systems referred to ALFC & AGC</p> <ul style="list-style-type: none"> - Hydraulic amplifier. - Frequency integrator - Governor - Comparator <p>Functions of following systems referred to ALFC & AGC</p> <ul style="list-style-type: none"> • Hydraulic amplifier: It comprises a pilot valve and main piston arrangement low power level pivot valve movement is connected into high power level piston valve movement. This is necessary in order to open or close the steam valve against high pressure stream. • Frequency integrator: It converts frequency signal into speed signal. • Governor: It raises the signal to increase or decrease the speed of turbine through link mechanism. 	<p>4M</p> <p style="text-align: right;"><i>Each</i> function <i>1M</i></p>



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		<ul style="list-style-type: none">• Comparator: It compares the actual frequency with the reference frequency and sends the signal to Frequency integrator.	
(d) Ans.	State the necessity of load forecasting in power system operation. Necessity of Load forecasting: Load forecasting for power system operation is required ... <ol style="list-style-type: none">1. For proper planning, designing of new power system network or expansion of existing.2. For varying generation of power with respect to time i.e. amount of growth expected in power demand.3. For determining the capacity of power generation and power flow through transmission lines and distribution lines.4. For proper planning of power flow through transmission & distribution network.5. For proper operation of power system in instability condition.6. For proper planning of resources for generation of power i.e. conventional or non-conventional resources.7. For determining the cost of power generation, transmission and distribution.8. For proper man power development or training of manpower for operation of power system.9. To decide power tariff for different utilities and different consumers.10. For proper power transaction between neighbouring grid system.11. For proper energy sales in electrical market.12. For finding the requirement of fuel in future.	4M <i>Any four necessity 1M each</i>	
(e) Ans.	“Load shedding is adopted during the operation of power system”. Give reason. Load shedding means intentional interruption of supply to load. The reasons for adopting load shedding during power system operation are <ol style="list-style-type: none">1. To keep balance between power demand and power generation.2. To maintain the stability condition of system due to sudden rise or fall in demand/load.3. To overcome energy generation crises / lack of generated energy.4. Sharing of power so to increase run time of critical loads.5. To reduce wastage of energy and max demand.6. To adopt energy conversation objectives.7. To reduce peak demand charges and also to reduce energy bills.	4M <i>Any Four reasons 1M each</i>	



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(f)	Refer to Indian power system scenario state the types of LDC and their locations.		4M																										
	Ans.	<p>For the efficient, economical and integrated transmission of electrical supply, the central government has made region wise demarcation of the country and has established load dispatch centers.</p> <p>Indian power system has identified different types of LDC depending on their locations.</p> <ol style="list-style-type: none"> 1. National Load Dispatch Centre (NLDC) 2. In India NLDS is located at Delhi 3. Regional Load Dispatch Centre (RLDC) 4. State Level Load Dispatch Centre (SLDC) 5. Sub State Load Dispatch Centre (SSLDC) 6. Local are LDC <p>Types of LDC:</p> <table border="1" style="width: 100%; border-collapse: collapse; margin-left: 20px;"> <thead> <tr> <th colspan="2" style="text-align: center;">Types of LDC</th> <th style="text-align: center;">Locations</th> </tr> </thead> <tbody> <tr> <td colspan="2">National Load Dispatch Centre (NLDC)</td> <td style="text-align: center;">Delhi</td> </tr> <tr> <td rowspan="5" style="text-align: center; vertical-align: middle;">RLDC</td> <td>ERLDC – Eastern Region</td> <td style="text-align: center;">Kolkata</td> </tr> <tr> <td>SRLDC – Southern Region</td> <td style="text-align: center;">Bangalore</td> </tr> <tr> <td>WRLDC – Western Region</td> <td style="text-align: center;">Mumbai (Kalwa)</td> </tr> <tr> <td>NELDC – North East Region</td> <td style="text-align: center;">Shilong</td> </tr> <tr> <td>NRLDC – Northern Region</td> <td style="text-align: center;">Delhi</td> </tr> <tr> <td style="text-align: center; vertical-align: middle;">SLDC -State Level Load Dispatch Centre</td> <td>Maharashtra state LDC</td> <td style="text-align: center;">Nagpur</td> </tr> <tr> <td style="text-align: center; vertical-align: middle;">SSLDC- Sub State Load Dispatch Centre</td> <td>Maharashtra state LDC</td> <td style="text-align: center;">Mumbai</td> </tr> <tr> <td style="text-align: center; vertical-align: middle;">LLDC – Local Load Dispatch Centre</td> <td>Tata Power Company Ltd</td> <td style="text-align: center;">Mumbai</td> </tr> </tbody> </table>	Types of LDC		Locations	National Load Dispatch Centre (NLDC)		Delhi	RLDC	ERLDC – Eastern Region	Kolkata	SRLDC – Southern Region	Bangalore	WRLDC – Western Region	Mumbai (Kalwa)	NELDC – North East Region	Shilong	NRLDC – Northern Region	Delhi	SLDC -State Level Load Dispatch Centre	Maharashtra state LDC	Nagpur	SSLDC- Sub State Load Dispatch Centre	Maharashtra state LDC	Mumbai	LLDC – Local Load Dispatch Centre	Tata Power Company Ltd	Mumbai	<i>1M for each type with location</i>
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6.	(a)	<p>Attempt any FOUR:</p> <p>Refer to Y_{bus} matrix, define</p> <ul style="list-style-type: none"> - driving point admittance - transfer admittance 	16 4M																										
	Ans.																												



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$$Y_{bus} = \begin{bmatrix} Y_{11} & Y_{12} & \dots & Y_{1n} \\ Y_{21} & Y_{22} & \dots & Y_{2n} \\ Y_{n1} & Y_{n2} & \dots & Y_{nn} \end{bmatrix}$$

Driving point admittance: The diagonal elements of Y_{bus} matrix are called **driving point admittance or self-admittance**. It is the sum of line charging admittance of a bus and line admittance between that bus other connecting buses to it.

$$\therefore y_{11} = y_{10} + y_{12} + y_{13}$$

$$y_{22} = y_{20} + y_{21} + y_{23}$$

$$y_{33} = y_{30} + y_{31} + y_{32}$$

Transfer admittance: The off diagonal elements of Y_{bus} are called as transfer admittance or mutual admittance. It is the line admittance between a bus and other bus with negative sign.

$$y_{12} = y_{21} = -y_{12}$$

$$y_{13} = y_{31} = -y_{13}$$

$$y_{14} = -y_{41}$$

$$y_{23} = y_{32} = -y_{23}$$

OR

*Each
definition
2M*



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Y_{bus} matrix for a 3 bus system can be obtained from power system equations.

$$I_1 = Y_{11}V_1 + Y_{12}V_2 + Y_{13}V_3 \quad \text{--- (1)}$$

$$I_2 = Y_{21}V_1 + Y_{22}V_2 + Y_{23}V_3 \quad \text{--- (2)}$$

$$I_3 = Y_{31}V_1 + Y_{32}V_2 + Y_{33}V_3 \quad \text{--- (3)}$$

From eq. (1), we can define

$$Y_{11} = \frac{I_1}{V_1} \Big|_{V_2=V_3=0} \quad \text{--- It is the self-admittance of bus-1 when bus-2 & bus-3 are shorted to reference node, i.e. } V_2=V_3=0.$$

$$\text{Similarly } Y_{22} = \frac{I_2}{V_2} \Big|_{V_1=V_3=0} \quad Y_{33} = \frac{I_3}{V_3} \Big|_{V_1=V_2=0}$$

$Y_{12} = \frac{-I_1}{V_2} \Big|_{V_1=V_3=0}$. It is the mutual admittance between bus-1 & bus-2 and is measured by injecting current I_2 in bus-2 and shorting the bus-1 & bus-3 to reference node. Now $I_1=0$ but I_2 flows in opposite direction, i.e. $I_1 = -I_2$. \therefore This admittance is considered with negative sign.

$$Y_{21} = \frac{I_2}{V_1} \Big|_{V_2=V_3=0} \quad \text{here } I_2 = -I_1$$

Also $Y_{12} = Y_{21}$ can be written as
 Y_{bus} matrix

$$Y_{bus} = \begin{pmatrix} Y_{11} & Y_{12} & Y_{13} \\ Y_{21} & Y_{22} & Y_{23} \\ Y_{31} & Y_{32} & Y_{33} \end{pmatrix}$$

All diagonal elements are self-admittance and off-diagonal elements are mutual admittance.
 \therefore is useful for



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	<p>(b) With the help of diagram explain voltage control by - tap changing transformer - Booster transformer</p> <p>Ans. Following are the different types of transformers used for voltage control in power system.</p> <p>1) Online tap changing transformer: All transformers are provided with taps on the winding for adjusting the ratio of transformation. Taps are usually provided on the high voltage winding to enable a fine control of voltage. Generally the tap changing can be done any when the transformer is in de-energized state. However in some cases tap changing is also possible when the transformer is energized. These transformers make it possible to maintain a constant voltage level on important buses in the system.</p> <p>Location: Intermediate distribution Substation</p> <p>2) Off load tap-changing transformer: Figure shows the arrangement where a number of tapings have been provided on the secondary. As the position of the tap is varied, the effective number of secondary turns is varied and hence the output voltage of the secondary can be changed. Thus referring to figure when the movable arm makes contact with stud 1, the secondary voltage is minimum and when with stud 5, it is maximum. During the period of light load, the voltage across the primary is not much below the alternator voltage and the movable arm is placed on stud 1. When the load increases, the voltage across the primary drops, but the secondary voltage can be kept at the previous value by placing the movable arm on to a higher stud. Whenever a tapping is to be changed in this type of transformer, the load is kept off and hence the name off load tap-changing transformer.</p> <div data-bbox="495 1522 1156 1753" data-label="Diagram"></div>	<p>4M</p> <p><i>Tap changing 2M</i></p>
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		<p>achieved by the use of booster transformer. The secondary of booster transformer is connected in series with the line whose voltage is to be controlled. The primary of this transformer is supplied from a regulating transformer with on load tap changing gear. Location: HV &EHV transmission Line</p>	<p>Booster 2M</p>
<p>(c) Ans.</p>	<p>Explain the concept of single area control referred to Load frequency control. In power system network “single area” is identified as grid network consisting number of generators supply power to all consumers in that area. Stability is concerned with this area only. Power demand and supply observed for this area only. All generators are connected in parallel in synchronism and shares the load. The system can be modelled as below:</p>		<p style="text-align: center;">4M</p> <p style="text-align: right;">Explan ation 3M</p>
			<p>Diagram 1M</p>
	<ul style="list-style-type: none"> . The above fig shows the block diagram representation of load frequency control. . Due to change in frequency of load side the system become unstable. To make system again in to stable condition load frequency control system is adopted. . The change in frequency is sense by frequency sensor and compared it with the reference frequency. . If the frequency change occurs that signal is send to the steam valve controller. The steam value controller will adjust the opening and closing of steam. 		



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		<p>the correlation between weather parameters and model their influence on power assumption.</p> <p>3. Temperature & wind speed/direction affects the heating /air conditioning loads. Cloud, humidity, fog affects lighting load as they affect the day-light illumination. Temperature & load has non-linear relationship. In a typical season changes in temp is 1⁰C, then change in load demand will be by 1%.</p> <p>4. Random weather change: Storm, heavy rain, flood, sunami etc. Sudden change in weather will affect the infrastructure of the power system and there by large disturbance takes place and load demand varies. So weather forecast, are to be considered while forecasting power loads.</p>	
<p>(e) Ans.</p>	<p>Draw and explain the incremental fuel cost curve.</p> <p>Definition:-Incremental fuel cost curve is graphical representation of relation between costs of incremental fuel input with the power output in MW.</p> <p>Incremental production cost = Incremental cost power generation = incr. cost of fuel + incr. cost of labour + incr. cost of transportation + incr. cost of water supply+ incr. cost of taxes</p> <p>Practically it is difficult to develop the relation between incr. cost of labour, incr. cost of transportation, incr. cost of water supply, incr. cost of taxes with the power o/p and represent it in mathematical form.. And also they are negligible compare to incremental fuel cost. Therefore we get</p> <p>Incremental production cost = Incremental fuel cost = $\frac{dF}{dP} = \lambda$</p> <p>Incremental fuel cost curve is a wide concave curve which shows that as power output is increases increment fuel cost also increases. In the lower range of power output, rise in incremental fuel cost is much smaller than that in the higher range of power output. Pmax & Pmin indicates max & min. power generation limits.</p>	<p style="text-align: center;">4M</p> <p style="text-align: center;"><i>1M for Diagram</i> , <i>1M for equation and</i></p> <p style="text-align: center;"><i>Explanation 2M</i></p>	
		<p>The graph shows a concave curve representing the incremental fuel cost. The vertical axis is labeled 'Incr. fuel i/p in Kcal /hr or Rs / hr' and the horizontal axis is 'Power o/p in Mw'. A tangent line is drawn at a point on the curve, with its slope labeled as 'slope=Fm'. The slope is also labeled as lambda (λ). The minimum power output is labeled as Pmin.</p>	



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	<p>$\therefore P_1 = 163.63 \text{ MW}$</p> <p>$\therefore$ From equation (i)</p> <p>$P_1 + P_2 = 410 \quad \therefore P_2 = 410 - 163.63 = 246.37 \text{ MW}$</p> <p>$\therefore$ Load distribution is <input type="text" value="P<sub>1</sub> = 163.63MW"/></p> <p><input type="text" value="P<sub>2</sub> = 246.37MW"/></p>	<p><i>1M</i></p> <p><i>1M</i></p>
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